

# ICC-ES Evaluation Report ESR-3814



Reissued January 2023

Revised March 2023

This report is subject to renewal January 2025.

www.icc-es.org | (800) 423-6587 | (562) 699-0543

A Subsidiary of the International Code Council®

DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-installed Concrete Anchors

**REPORT HOLDER:** 

HILTI, INC.

#### **EVALUATION SUBJECT:**

HILTI HIT-RE 500 V3 ADHESIVE ANCHORS AND POST-INSTALLED REINFORCING BAR CONNECTIONS IN CRACKED AND UNCRACKED CONCRETE

#### 1.0 EVALUATION SCOPE

#### Compliance with the following codes:

- 2021, 2018, 2015, and 2012 International Building Code<sup>®</sup> (IBC)
- 2021, 2018, 2015, and 2012 International Residential Code® (IRC)

For evaluation for compliance with the *National Building Code of Canada*® (NBCC), see listing report <u>ELC-3814</u>.

For evaluation for compliance with codes adopted by Los Angeles Department of Building and Safety (LADBS), see ESR-3814 LABC and LARC Supplement.

#### Property evaluated:

Structural

#### **2.0 USES**

The Hilti HIT-RE 500 V3 Adhesive Anchoring System and Post-Installed Reinforcing Bar System are used to resist static, wind and earthquake (Seismic Design Categories A through F) tension and shear loads in cracked and uncracked normal-weight and lightweight concrete having a specified compressive strength, f'c, of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

The anchor system complies with anchors as described in Section 1901.3 of the 2021, 2018 and 2015 IBC, and Section 1909 of the 2012 IBC and is an alternative to cast-in-place anchors described in Section 1908 of the 2012 IBC. The anchor systems may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the IRC.

The post-installed reinforcing bar system is an alternative to cast-in-place reinforcing bars governed by ACI 318 and IBC Chapter 19.

#### 3.0 DESCRIPTION

#### 3.1 General:

The Hilti HIT-RE 500 V3 Adhesive Anchoring System and Post-Installed Reinforcing Bar System are comprised of the following components:

- Hilti HIT-RE 500 V3 adhesive packaged in foil packs
- Adhesive mixing and dispensing equipment
- Equipment for hole cleaning and adhesive injection

The Hilti HIT-RE 500 V3 Adhesive Anchoring System may be used with continuously threaded rod, Hilti HIS-(R)N internally threaded inserts or deformed steel reinforcing bars as depicted in Figure 4. The Hilti HIT-RE 500 V3 Post-Installed Reinforcing Bar System may only be used with deformed steel reinforcing bars as depicted in Figures 2 and 3. The primary components of the Hilti Adhesive Anchoring and Post-Installed Reinforcing Bar Systems, including the Hilti HIT-RE 500 V3 Adhesive, HIT-RE-M static mixing nozzle and steel anchoring elements, are shown in Figure 7 of this report.

The manufacturer's printed Installation instructions (MPII), as included with each adhesive unit package, are consolidated as Figure 8A and 8B.

#### 3.2 Materials:

**3.2.1 Hilti HIT-RE 500 V3 Adhesive:** Hilti HIT-RE 500 V3 Adhesive is an injectable, two-component epoxy adhesive. The two components are separated by means of a dual-cylinder foil pack attached to a manifold. The two components combine and react when dispensed through a static mixing nozzle attached to the manifold. Hilti HIT-RE 500 V3 is available in 11.1-ounce (330 ml), 16.9-ounce (500 ml), and 47.3-ounce (1400 ml) foil packs. The manifold attached to each foil pack is stamped with the adhesive expiration date. The shelf life, as indicated by the expiration date, applies to an unopened foil pack stored in a dry, dark environment and in accordance with Figure 8A.

#### 3.2.2 Hole Cleaning Equipment:

**3.2.2.1 Standard Equipment:** Standard hole cleaning equipment, comprised of steel wire brushes and air nozzles, is described in Figure 8A of this report.

**3.2.2.2 Hilti Safe-Set™ System:** For the elements described in Sections 3.2.5.1 through 3.2.5.3 and Section 3.2.6, the Hilti TE-CD or TE-YD hollow carbide drill bit with a carbide drilling head conforming to ANSI B212.15 must be used. When used in conjunction with a Hilti vacuum with a minimum value for the maximum volumetric flow rate of 129 CFM (61 ℓ/s), the Hilti TE-CD or TE-YD drill bit will



remove the drilling dust, automatically cleaning the hole. Available sizes for Hilti TE-CD or TE-YD drill bit are shown in Figure 8A.

#### 3.2.3 Hole Preparation Equipment:

- **3.2.3.1** Hilti Safe-Set™ System: TE-YRT Roughening Tool: For the elements described in Sections 3.2.5.1 through 3.2.5.3 and Tables 9, 12, 17, 20, and 29, the Hilti TE-YRT roughening tool with a carbide roughening head is used for hole preparation in conjunction with holes core drilled with a diamond core bit as illustrated in Figure 5.
- **3.2.4 Dispensers:** Hilti HIT-RE 500 V3 must be dispensed with manual, electric, or pneumatic dispensers provided by Hilti.

#### 3.2.5 Anchor Elements:

- **3.2.5.1 Threaded Steel Rods:** Threaded steel rods must be clean, continuously threaded rods (all-thread) in diameters as described in Tables 6 and 14 and Figure 4 of this report. Steel design information for common grades of threaded rods is provided in Table 2. Carbon steel threaded rods must be furnished with a 0.0002-inch-thick (0.005 mm) zinc electroplated coating complying with ASTM B633 SC 1 or must be hot-dipped galvanized complying with ASTM A153, Class C or D. Stainless steel threaded rods must comply with ASTM F593 or ISO 3506 A4. Threaded steel rods must be straight and free of indentations or other defects along their length. The ends may be stamped with identifying marks and the embedded end may be blunt cut or cut on the bias to a chisel point.
- **3.2.5.2** Steel Reinforcing Bars for use in Post-Installed Anchor Applications: Steel reinforcing bars are deformed bars as described in Table 3 of this report. Tables 6, 14, and 22 and Figure 4 summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be straight, and free of mill scale, rust, mud, oil, and other coatings (other than zinc) that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation, except as set forth in ACI 318-19 Section 26.6.3.2(b), ACI 318-14 Section 26.6.3.1(b) or ACI 318-11 Section 7.3.2, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.
- 3.2.5.3 Hilti HIS-N and HIS-RN Inserts: Hilti HIS-N and HIS-RN inserts have a profile on the external surface and are internally threaded. Mechanical properties for Hilti HIS-N and HIS-RN inserts are provided in Table 4. The inserts are available in diameters and lengths as shown in Table 26 and Figure 4. Hilti HIS-N inserts are produced from carbon steel and furnished with a 0.0002-inch-thick (0.005 mm) zinc electroplated coating complying with ASTM SC 1. The stainless steel Hilti HIS-RN inserts are fabricated from X5CrNiMo17122 K700 steel conforming to DIN 17440. Specifications for common bolt types that may be used in conjunction with Hilti HIS-N and HIS-RN inserts are provided in Table 5. Bolt grade and material type (carbon, stainless) must be matched to the insert. Strength reduction factors,  $\phi$ , corresponding to brittle steel elements must be used for Hilti HIS-N and HIS-RN inserts.
- **3.2.5.4 Ductility:** In accordance with ACI 318 (-19 and -14) 2.3 or ACI 318-11 D.1, as applicable, in order for a steel element to be considered ductile, the tested elongation must be at least 14 percent and reduction of area must be at least 30 percent. Steel elements with a tested elongation of less than 14 percent or a reduction of area of less than 30 percent, or both, are considered brittle. Values for various steel materials are provided in Tables 2, 3, 4, and 5 of this report. Where values are nonconforming or unstated, the steel must be considered brittle.

**3.2.6 Steel Reinforcing Bars for Use in Post-Installed Reinforcing Bar Connections:** Steel reinforcing bars used in post-installed reinforcing bar connections are deformed bars (rebar) as depicted in Figures 2 and 3. Tables 31, 32, 33, and Figure 4 summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be straight, and free of mill scale, rust, mud, oil, and other coatings that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation, except as set forth in Section 26.6.3.2(b) of ACI 318-19, ACI 318-14 26.6.3.1(b) or ACI 318-11 7.3.2, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.

#### 3.3 Concrete:

Normal-weight or lightweight concrete must comply with Sections 1903 and 1905 of the IBC, as applicable. The specified compressive strength of the concrete must be from 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

#### 4.0 DESIGN AND INSTALLATION

#### 4.1 Strength Design of Post-Installed Anchors:

Refer to Table 1 for the design parameters for specific installed elements, and refer to Figure 5 and Section 4.1.4 for a flowchart to determine the applicable design bond strength or pullout strength.

**4.1.1 General:** The design strength of anchors under the 2021 IBC, as well as the 2021 IRC, must be determined in accordance with ACI 318-19 and this report. The design strength of anchors complying with the 2018 and 2015 IBC, as well as Section R301.1.3 of the 2018 and 2015 IRC must be determined in accordance with ACI 318-14 Chapter 17 and this report.

The design strength of anchors under the 2012 IBC, as well as the 2012 IRC must be determined in accordance with ACI 318-11 and this report.

Design parameters are based on ACI 318-19 for use with the 2021 IBC, ACI 318-14 for use with the 2018 and 2015 IBC, and ACI 318-11 for use with the 2012 IBC unless noted otherwise in Sections 4.1.1 through 4.1.11 of this report.

The strength design of anchors must comply with ACI 318-19 17.5.1.2, ACI 318-14 17.3.1 or ACI 318-11 D.4.1 as applicable, except as required in ACI 318-19 17.10, ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable.

Design parameters are provided in Table 6A through Table 30. Strength reduction factors,  $\phi$ , as given in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, must be used for load combinations calculated in accordance with Section 1605.1 of the 2021 IBC, Section 1605.2 of the 2018, 2015, and 2012 IBC or ACI 318 (-19 and -14) 5.3 or ACI 318-11 9.2, as applicable. Strength reduction factors,  $\phi$ , as given in ACI 318-11 D.4.4 must be used for load combinations calculated in accordance with ACI 318-11 Appendix C.

- **4.1.2 Static Steel Strength in Tension:** The nominal static steel strength of a single anchor in tension,  $N_{\rm Se}$ , in accordance with ACI 318-19 17.6.1.2, ACI 318-14 17.4.1.2 or ACI 318-11 Section D.5.1.2, as applicable, and the associated strength reduction factors,  $\phi$ , in accordance with ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 Section D.4.3, as applicable, are provided in the tables outlined in Table 1 for the anchor element types included in this report.
- **4.1.3 Static Concrete Breakout Strength in Tension:** The nominal concrete breakout strength of a single anchor or group of anchors in tension,  $N_{cb}$  or  $N_{cbg}$ , must be calculated in accordance with ACI 318-19 17.6.2, ACI 318-14 17.4.2 or ACI 318-11 D.5.2, as applicable, with the following addition:

The basic concrete breakout strength of a single anchor in tension,  $N_b$ , must be calculated in accordance with ACI 318-19 17.6.2.2, ACI 318-14 17.4.2.2 or ACI 318-11 D.5.2.2, as applicable using the values of  $k_{c,cr}$ , and  $k_{c,uncr}$ , as described in this report. Where analysis indicates no cracking in accordance with ACI 318-19 17.6.2.5, ACI 318-14 17.4.2.6 or ACI 318-11 D.5.2.6, as applicable,  $N_b$  must be calculated using  $k_{c,uncr}$  and  $\Psi_{c,N}$  = 1.0. See Table 1. For anchors in lightweight concrete, see ACI 318-19 17.2.4, ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable. The value of  $f_c$  used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318-19 17.3.1, ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable. Additional information for the determination of nominal bond strength in tension is given in Section 4.1.4 of this report.

**4.1.4 Static Bond Strength in Tension:** The nominal static bond strength of a single adhesive anchor or group of adhesive anchors in tension,  $N_a$  or  $N_{ag}$ , must be calculated in accordance with ACI 318-19 17.6.5, ACI 318-14 17.4.5 or ACI 318-11 D.5.5, as applicable. Bond strength values are a function of the concrete compressive strength, whether the concrete is cracked or uncracked, the concrete temperature range, the drilling method, and the installation conditions (dry or water-saturated, etc.). The resulting characteristic bond strength shall be multiplied by the associated strength reduction factor  $\phi_{nn}$  as follows:

	•		•	
DRILLING METHOD	CONCRETE TYPE	PERMISSIBLE INSTALLATION CONDITIONS BOND STRENGTH		ASSOCIATED STRENGTH REDUCTION FACTOR
		Dry	Tk,uncr or Tk,cr	Фа
Hammer-drill	Cracked and	Water-saturated	Tk,uncr or Tk,cr	<b>ø</b> ws
	Uncracked	Water-filled hole	$\mathcal{T}_{k,uncr}$ or $\mathcal{T}_{k,cr}$	фwf
		Underwater application	Tk,uncr or Tk,cr	$\phi_{ m uw}$
Core Drilled with Roughening Tool	Cracked and	Dry	Tk,uncr or Tk,cr	Фа
or Hilti TE-CD or TE-YD Hollow Drill Bit	-	Water-saturated	$\mathcal{T}_{k,uncr}$ or $\mathcal{T}_{k,cr}$	<b>Ø</b> ws
Cara Drill	I In ava also d	Dry	Tk,uncr	$\phi_{ extsf{d}}$
Core Drilled	Uncracked	Water-saturated	$ au_{k,uncr}$	<i>φ</i> ws

Figure 5 of this report presents a bond strength design selection flowchart. Strength reduction factors for determination of the bond strength are outlined in Table 1 of this report. Adjustments to the bond strength may also be made for increased concrete compressive strength as noted in the footnotes to the bond strength tables.

- **4.1.5** Static Steel Strength in Shear: The nominal static strength of a single anchor in shear as governed by the steel,  $V_{sa}$ , in accordance with ACI 318-19 17.7.1.2, ACI 318-14 17.5.1.2 or ACI 318-11 D.6.1.2, as applicable, and strength reduction factors,  $\phi$ , in accordance with ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are given in the tables outlined in Table 1 for the anchor element types included in this report.
- **4.1.6 Static Concrete Breakout Strength in Shear:** The nominal static concrete breakout strength of a single anchor or group of anchors in shear,  $V_{cb}$  or  $V_{cbg}$ , must be calculated in accordance with ACI 318-19 17.7.2, ACI 318-14 17.5.2 or ACI 318-11 D.6.2, as applicable, based on information

given in the tables outlined in Table 1. The basic concrete breakout strength of a single anchor in shear,  $V_b$ , must be calculated in accordance with ACI 318-19 17.7.2.2, ACI 318-14 17.5.2.2 or ACI 318-11 D.6.2.2, as applicable, using the values of d given in the tables as outlined in Table 1 for the corresponding anchor steel in lieu of  $d_a$  (2021, 2018, 2015, and 2012 IBC). In addition,  $h_{ef}$  must be substituted for  $\ell_e$ . In no case must  $\ell_e$  exceed 8d. The value of  $f_c$  must be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318-19 17.3.1, ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable.

- **4.1.7 Static Concrete Pryout Strength in Shear:** The nominal static pryout strength of a single anchor or group of anchors in shear,  $V_{cp}$  or  $V_{cpg}$ , must be calculated in accordance with ACI 318-19 17.7.3, ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable.
- **4.1.8 Interaction of Tensile and Shear Forces: For** designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-19 17.8, ACI 318-14 17.6 or ACI 318-11 D.7, as applicable.
- **4.1.9 Minimum Member Thickness,**  $h_{min}$ , **Anchor Spacing,**  $s_{min}$  and Edge Distance,  $c_{min}$ : In lieu of ACI 318-19 17.9.2, ACI 318-14 17.7.1 and 17.7.3 or ACI 318-11 D.8.1 and D.8.3, as applicable, values of  $s_{min}$  and  $c_{min}$  described in this report must be observed for anchor design and installation. Likewise, in lieu of ACI 318-19 17.9.4, ACI 318-14 17.7.5 or ACI 318-11 D.8.5, as applicable, the minimum member thicknesses,  $h_{min}$ , described in this report must be observed for anchor design and installation. For adhesive anchors that will remain untorqued, ACI 318-19 17.9.3, ACI 318-14 17.7.4 or ACI 318-11 D.8.4, as applicable, applies.

For edge distances  $c_{ai}$  and anchor spacing  $s_{ai}$ , the maximum torque  $T_{max}$  shall comply with the following requirements:

REDUCED MAXIMUM INSTALLATION TORQUE $T_{max,red}$ FOR EDGE DISTANCES $c_{ai} < (5 \times d_a)$					
EDGE DISTANCE, $c_{ai}$ MINIMUM ANCHOR MAXIMUM TORQUE, SPACING, $s_{ai}$ $T_{max,red}$					
1.75 in. (45 mm) ≤ c <sub>ai</sub>	$5 \times d_a \le s_{ai} < 16 \text{ in.}$	0.3 x <i>T<sub>max</sub></i>			
< 5 x d <sub>a</sub>	s <sub>ai</sub> ≥ 16 in. (406 mm)	0.5 x T <sub>max</sub>			

**4.1.10 Critical Edge Distance**  $c_{ac}$ : In lieu of ACI 318-19 17.9.5, ACI 318-14 17.7.6 or ACI 318-11 D.8.6, as applicable,  $c_{ac}$  must be determined as follows:

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k,uncr}}{1160}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$
 Eq. (4-1)

where 
$$\left[\frac{h}{h_{ef}}\right]$$
 need not be taken as larger than 2.4: and

 $\tau_{k,uncr}$  is the characteristic bond strength in uncracked concrete stated in the tables of this report, whereby  $\tau_{k,uncr}$  need not be taken as greater than:

$$\tau_{k,uncr} = \frac{k_{uncr} \sqrt{h_{ef} \dot{f}_c}}{\pi \cdot d_a}$$

**4.1.11 Design Strength in Seismic Design Categories C, D, E and F:** In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, the design must be performed according to ACI 318-19 17.10, ACI 318-14 17.2.3 or ACI 318-11 Section D.3.3, as applicable. Modifications to ACI 318-19 17.10 and ACI 318-14 17.2.3 shall be applied under Section 1905.1.8 of the 2021, 2018 and 2015 IBC. For the 2012 IBC, Section 1905.1.9 shall be omitted.

The nominal steel shear strength,  $V_{sa}$ , must be adjusted by  $\alpha_{V,seis}$  as given in the tables summarized in Table 1 for the anchor element types included in this report. For tension, the nominal pullout strength  $N_{p,cr}$  or bond strength  $\tau_{cr}$  must be adjusted by  $\alpha_{N,seis}$ . See Tables 8, 9, 11, 12, 16, 17, 19, 20, 24, 28 and 29.

Modify ACI 318-11 Sections D.3.3.4.2, D.3.3.4.3(d) and D.3.3.5.2 to read as follows:

ACI 318-11 D.3.3.4.2 - Where the tensile component of the strength-level earthquake force applied to anchors exceeds 20 percent of the total factored anchor tensile force associated with the same load combination, anchors and their attachments shall be designed in accordance with ACI 318-11 D.3.3.4.3. The anchor design tensile strength shall be determined in accordance with ACI 318-11 D.3.3.4.4

#### Exception:

1. Anchors designed to resist wall out-of-plane forces with design strengths equal to or greater than the force determined in accordance with ASCE 7 Equation 12.11-1 or 12.14-10 shall be deemed to satisfy ACI 318-11 D.3.3.4.3(d).

ACI 318-11 D.3.3.4.3(d) – The anchor or group of anchors shall be designed for the maximum tension obtained from design load combinations that include E, with E increased by  $\Omega_0$ . The anchor design tensile strength shall be calculated from ACI 318-11 D.3.3.4.4.

ACI 318-11 D.3.3.5.2 – Where the shear component of the strength-level earthquake force applied to anchors exceeds 20 percent of the total factored anchor shear force associated with the same load combination, anchors and their attachments shall be designed in accordance with ACI 318-11 D.3.3.5.3. The anchor design shear strength for resisting earthquake forces shall be determined in accordance with ACI 318-11 D.6.

#### Exceptions:

- 1. For the calculation of the in-plane shear strength of anchor bolts attaching wood sill plates of bearing or non-bearing walls of light-frame wood structures to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:
  - 1.1. The allowable in-plane shear strength of the anchor is determined in accordance with AF&PA NDS Table 11E for lateral design values parallel to grain.
  - 1.2. The maximum anchor nominal diameter is  $\frac{5}{8}$  inch (16 mm).
  - 1.3. Anchor bolts are embedded into concrete a minimum of 7 inches (178 mm).
  - 1.4. Anchor bolts are located a minimum of  $1^{3}/_{4}$  inches (45 mm) from the edge of the concrete parallel to the length of the wood sill plate.
  - 1.5. Anchor bolts are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the wood sill plate.
  - 1.6. The sill plate is 2-inch or 3-inch nominal thickness.
- 2. For the calculation of the in-plane shear strength of anchor bolts attaching cold-formed steel track of bearing or non-bearing walls of light-frame construction to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3, need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:

- 2.1. The maximum anchor nominal diameter is  $^{5}/_{8}$  inch (16 mm).
- 2.2. Anchors are embedded into concrete a minimum of 7 inches (178 mm).
- 2.3. Anchors are located a minimum of  $1^{3}/_{4}$  inches (45 mm) from the edge of the concrete parallel to the length of the track.
- 2.4. Anchors are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the track.
- 2.5. The track is 33 to 68 mil designation thickness.

Allowable in-plane shear strength of exempt anchors, parallel to the edge of concrete shall be permitted to be determined in accordance with AISI S100 Section E3.3.1.

3. In light-frame construction, bearing or nonbearing walls, shear strength of concrete anchors less than or equal to 1 inch [25 mm] in diameter attaching a sill plate or track to foundation or foundation stem wall need not satisfy ACI 318-11 D.3.3.5.3(a) through (c) when the design strength of the anchors is determined in accordance with ACI 318-11 D.6.2.1(c).

## 4.2 Strength Design of Post-Installed Reinforcing Bars:

**4.2.1 General:** The design of straight post-installed deformed reinforcing bars must be determined in accordance with ACI 318 rules for cast-in place reinforcing bar development and splices and this report.

Examples of typical applications for the use of post-installed reinforcing bars are illustrated in Figures 2 and 3 of this report.

**4.2.2 Determination of bar development length**  $I_d$ : Values of  $I_d$  must be determined in accordance with the ACI 318 development and splice length requirements for straight cast-in place reinforcing bars.

#### Exceptions:

- 1. For uncoated and zinc-coated (galvanized) post-installed reinforcing bars, the factor  $\Psi_{\rm e}$  shall be taken as 1.0. For all other cases, the requirements in ACI 318-19 25.4.2.5, ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (b) shall apply.
- 2. When using alternate methods to calculate the development length (e.g., anchor theory), the applicable factors for post-installed anchors generally apply.
- **4.2.3 Minimum Member Thickness,** *h<sub>min</sub>*, **Minimum Concrete Cover,** *c<sub>c,min</sub>*, **Minimum Concrete Edge Distance,** *c<sub>b,min</sub>*, **Minimum Spacing,** *s<sub>b,min</sub>*: For post-installed reinforcing bars, there is no limit on the minimum member thickness. In general, all requirements on concrete cover and spacing applicable to straight cast-in bars designed in accordance with ACI 318 shall be maintained.

For post-installed reinforcing bars installed at embedment depths,  $h_{ef}$ , larger than 20d ( $h_{ef}$  > 20d), the minimum concrete cover shall be as follows:

REBAR SIZE	MINIMUM CONCRETE COVER, $c_{c,min}$
$d_b \le No. \ 6 \ (16 \ mm)$	1 <sup>3</sup> / <sub>16</sub> in. (30mm)
No. $6 < d_b \le No. 10$	1 <sup>9</sup> / <sub>16</sub> in.
$(16mm < d_b \le 32mm)$	(40mm)

The following requirements apply for minimum concrete edge and spacing for  $h_{ef} > 20d$ :

Required minimum edge distance for post-installed reinforcing bars (measured from the center of the bar):

$$c_{b,min} = d_0/2 + c_{c,min}$$

Required minimum center-to-center spacing between post-installed bars:

$$s_{b,min} = d_0 + c_{c,min}$$

Required minimum center-to-center spacing from existing (parallel) reinforcing:

$$s_{b,min} = d_b/2$$
 (existing reinforcing) +  $d_0/2$  +  $c_{c,min}$ 

All other requirements applicable to straight cast-in place bars designed in accordance with ACI 318 shall be maintained.

- **4.2.4** Design Strength in Seismic Design Categories C, D, E and F: In structures assigned to Seismic Category C, D, E or F under the IBC or IRC, design of straight post-installed reinforcing bars must take into account the provisions of ACI 318 (-19 or -14) Chapter 18 or ACI 318-11 Chapter 21, as applicable.
- **4.2.5 Design in Fire Resistive Construction:** For post-installed reinforcing bars, the relationship of bond stress to temperature under fire conditions for short term loading (including seismic), suitable for use in determining conformance with fire resistance rating requirements is as follows (see Figures 6A and 6B):

$$au_{fire(\theta)} = 1,137,318 \cdot \theta^{-1.47}$$
 (psi) 
$$au_{fire(\theta)} = 522.93 \cdot \theta^{-1.14}$$
 (N/mm2)

Where  $\theta$  is the temperature in the concrete at the post-installed reinforcing bar in °F (for psi) or °C (for N/mm²), as applicable.

For temperatures above  $\theta_{max}$  of 581 °F (305 °C),  $\tau_{fire}(\theta)$ =0. For load cases including sustained loads, with or without short term loading, multiply  $\tau_{fire}(\theta)$  by 0.93.

The bond stress,  $\tau_{fire}(\theta)$ , shall not exceed 1,090 psi (7.5 N/mm<sup>2</sup>).

Determination of the temperature in the concrete at the location of the post-installed reinforcing bar is dependent on the geometry of the concrete members under consideration, and its calculation is the responsibility of the design professional. The design professional shall use the bond strength / temperature curves in Figure 6 along with a determination of the temperature in the concrete appropriate for the member geometry under consideration to calculate the reinforcing bar development length  $I_d$ .

#### 4.3 Installation:

Installation parameters are illustrated in Figures 1 and 4. Installation must be in accordance with ACI 318-19 26.7.2, ACI 318-14 17.8.1 and 17.8.2 or ACI 318-11 D.9.1 and D.9.2, as applicable. Anchor and post-installed reinforcing bar locations must comply with this report and the plans and specifications approved by the code official. Installation of the Hilti HIT-RE 500 V3 Adhesive Anchor and Post-Installed Reinforcing Bar Systems must conform to the manufacturer's printed installation instructions (MPII) included in each unit package consolidated as Figures 8A and 8B of this report. The MPII contains additional requirements for combinations of drill hole depth, diameter, drill bit type, hole preparation, and dispensing tools.

The initial cure time,  $t_{cure,ini}$ , as noted in Figure 8A of this report, is intended for rebar applications only and is the time where rebar and concrete formwork preparation may continue. Between the initial cure time and the full cure time,  $t_{cure,final}$ , the adhesive has a limited load bearing capacity. Do not apply a torque or load on the rebar during this time

#### 4.4 Special Inspection:

Periodic special inspection must be performed where required in accordance with Section 1705.1.1 and Table 1705.3 of the 2021, 2018, 2015 and 2012 IBC, as applicable, and this report. The special inspector must be on the jobsite initially during anchor or post-installed reinforcing bar installation to verify anchor or post-installed reinforcing bar type and dimensions, concrete type, concrete compressive strength, adhesive identification and expiration date, hole dimensions, hole cleaning procedures, spacing, edge distances, concrete thickness, anchor or post-installed reinforcing bar embedment, tightening torque and adherence to the manufacturer's printed installation instructions.

The special inspector must verify the initial installations of each type and size of adhesive anchor or post-installed reinforcing bar by construction personnel on site. Subsequent installations of the same anchor or post-installed reinforcing bar type and size by the same construction personnel are permitted to be performed in the absence of the special inspector. Any change in the anchor or post-installed reinforcing bar product being installed or the personnel performing the installation requires an initial inspection. For ongoing installations over an extended period, the special inspector must make regular inspections to confirm correct handling and installation of the product.

Continuous special inspection of adhesive anchors or post-installed reinforcing bar installed in horizontal or upwardly inclined orientations to resist sustained tension loads shall be performed in accordance with ACI 318-19 26.13.3.2(e) and 26.7.1(j), ACI 318-14 17.8.2.4, 26.7.1(h), and 26.13.3.2(c) or ACI 318-11 D.9.2.4, as applicable.

Under the IBC, additional requirements as set forth in Sections 1705, 1706, and 1707 must be observed, where applicable.

#### 5.0 CONDITIONS OF USE

The Hilti HIT-RE 500 V3 Adhesive Anchor System and Post-Installed Reinforcing Bar System described in this report complies with, or is a suitable alternative to what is specified in, the codes listed in Section 1.0 of this report, subject to the following conditions:

- 5.1 Hilti HIT-RE 500 V3 Adhesive anchors and post-installed reinforcing bars must be installed in accordance with the manufacturer's printed installation instructions (MPII) as included in the adhesive packaging and consolidated as Figures 8A and 8B of this report.
- **5.2** The anchors and post-installed reinforcing bars must be installed in cracked and uncracked normal-weight concrete having a specified compressive strength  $f_c' = 2,500$  psi to 8,500 psi (17.2 MPa to 58.6 MPa).
- 5.3 The values of f'c used for calculation purposes must not exceed 8,000 psi (55.1 MPa).
- 5.4 The concrete shall have attained its minimum design strength prior to installation of the Hilti HIT-RE 500 V3 adhesive anchors or post-installed reinforcing bars.
- 5.5 Anchors and post-installed reinforcing bars must be installed in concrete base materials in holes drilled using carbide-tipped drill bits manufactured with the range of maximum and minimum drill-tip dimensions specified in ANSI B212.15-1994, or diamond core drill bits, as detailed in Figure 8A. Use of the Hilti TE-YRT Roughening Tool in conjunction with diamond core bits must be as detailed in Figure 8B.
- 5.6 Loads applied to the anchors must be adjusted in accordance with Section 1605.1 of the 2021 IBC or

- Section 1605.2 of the 2018, 2015 and 2012 IBC for strength design and in accordance with Section 1605.1 of the 2021 IBC or Section 1605.3 of the 2018, 2015, and 2012 IBC for allowable stress design.
- 5.7 Hilti HIT-RE 500 V3 adhesive anchors and post-installed reinforcing bars are recognized for use to resist short- and long-term loads, including wind and earthquake, subject to the conditions of this report.
- 5.8 In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchor strength must be adjusted in accordance with Section 4.1.11 of this report, and post-installed reinforcing bars must comply with section 4.2.4 of this report.
- 5.9 Hilti HIT-RE 500 V3 adhesive anchors and post-installed reinforcing bars are permitted to be installed in concrete that is cracked or that may be expected to crack during the service life of the anchor, subject to the conditions of this report.
- **5.10** Anchor strength design values must be established in accordance with Section 4.1 of this report.
- 5.11 Post-installed reinforcing bar development and splice length is established in accordance with Section 4.2 of this report.
- 5.12 Minimum anchor spacing and edge distance as well as minimum member thickness must comply with the values noted in this report.
- 5.13 Post-installed reinforcing bar spacing, minimum member thickness, and cover distance must be in accordance with the provisions of ACI 318 for cast-in place bars and section 4.2.3 of this report.
- 5.14 Prior to anchor installation, calculations and details demonstrating compliance with this report must be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- 5.15 Anchors and post-installed reinforcing bars are not permitted to support fire-resistive construction. Where not otherwise prohibited by the code, Hilti HIT-RE 500 V3 adhesive anchors and post-installed reinforcing bars are permitted for installation in fire-resistive construction provided that at least one of the following conditions is fulfilled:
  - Anchors and post-installed reinforcing bars are used to resist wind or seismic forces only.
  - Anchors and post-installed reinforcing bars that support gravity load-bearing structural elements are within a fire-resistive envelope or a fire-resistive membrane, are protected by approved fire-resistive materials, or have been evaluated for resistance to fire exposure in accordance with recognized standards.
  - Anchors and post-installed reinforcing bars are used to support nonstructural elements.
  - Post-installed reinforcing bars designed in accordance with Section 4.2.5 of this report.
- 5.16 Since an ICC-ES acceptance criteria for evaluating data to determine the performance of adhesive anchors and post-installed reinforcing bars subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- **5.17** Use of zinc-plated carbon steel threaded rods or steel reinforcing bars is limited to dry, interior locations.

- 5.18 Use of hot-dipped galvanized carbon steel and stainless steel rods is permitted for exterior exposure or damp environments.
- 5.19 Steel anchoring materials in contact with preservative-treated and fire-retardant-treated wood must be of zinc-coated carbon steel or stainless steel. The minimum coating weights for zinc-coated steel must comply with ASTM A153. Periodic special inspection must be provided in accordance with Section 4.4 of this report. Continuous special inspection for anchors and post-installed reinforcing bars installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be provided in accordance with Section 4.4 of this report.
- 5.20 Installation of anchors and post-installed reinforcing bars in horizontal or upwardly inclined orientations to resist sustained tension loads shall be performed by personnel certified by an applicable certification program in accordance with ACI 318-19 26.7.2(e), ACI 318-14 17.8.2.2 or 17.8.2.3, or ACI 318-11 D.9.2.2 or D.9.2.3, as applicable.
- 5.21 Hilti HIT-RE 500 V3 adhesive anchors and post-installed reinforcing bars may be used to resist tension and shear forces in floor, wall, and overhead installations only if installation is into concrete with a temperature between 23°F and 104°F (-5°C and 40°C) for threaded rods, rebar, and Hilti HIS-(R)N inserts. Overhead installations for hole diameters larger than <sup>7</sup>/<sub>16</sub>-inch or 10mm require the use of piston plugs (HIT-SZ, -IP) during injection to the back of the hole. <sup>7</sup>/<sub>16</sub>-inch or 10mm diameter holes may be injected directly to the back of the hole with the use of extension tubing on the end of the nozzle. The anchor or post-installed reinforcing bars must be supported until fully cured (i.e., with Hilti HIT-OHW wedges, or other suitable means). Where temporary restraint devices are used, their use shall not result in imparement of the anchor shear resistance. Installations in concrete temperatures below 41°F (5°C) require the adhesive to be conditioned to a minimum temperature of 41°F (5°C).
- 5.22 Anchors and post-installed reinforcing bars shall not be used for applications where the concrete temperature can rise from 40°F or less to 80°F or higher within a 12-hour period. Such applications may include but are not limited to anchorage of building façade systems and other applications subject to direct sun exposure.
- **5.23** Hilti HIT-RE 500 V3 adhesives are manufactured by Hilti GmbH, Kaufering, Germany, under a quality-control program with inspections by ICC-ES.
- 5.24 Hilti HIS-N and HIS-RN inserts are manufactured by Hilti (China) Ltd., Guangdong, China, under a quality-control program with inspections by ICC-ES.

#### 6.0 EVIDENCE SUBMITTED

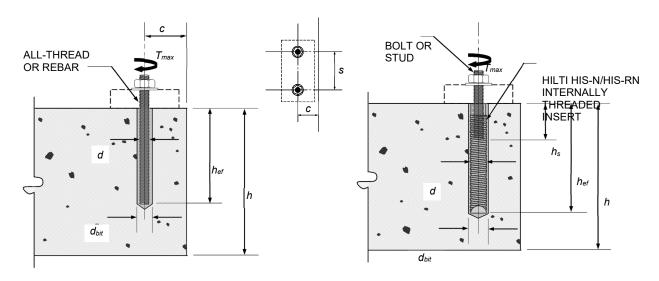
Data in accordance with the ICC-ES Acceptance Criteria for Post-installed Adhesive Anchors and Reinforcing Bars in Concrete Elements (AC308), dated October 2022, which incorporates requirements in ACI 355.4 (-19 and -11), including but not limited to tests under freeze/thaw conditions (Table 3.2, test series 6), and Table 3.8 for evaluating post-installed reinforcing bars including test series 15 for effects of fire on bond stress.

#### 7.0 IDENTIFICATION

7.1 The ICC-ES mark of conformity, electronic labeling, or the evaluation report number (ICC-ES ESR-3814) along with the name, registered trademark, or registered logo of the report holder must be included in the product label.

- **7.2** In addition, Hilti HIT-RE 500 V3 adhesive is identified by packaging labeled with the manufacturer's name (Hilti Corp.) and address, product name, lot number, expiration date.
- 7.3 Hilti HIS-N and HIS-RN inserts are identified by packaging labeled with the manufacturer's name (Hilti Corp.) and address, anchor name and size, and evaluation report number (ESR-3814). Threaded rods, nuts, washers, bolts, cap screws, and deformed reinforcing bars are standard elements and must conform to applicable national or international specifications.
- **7.4** The report holder's contact information is the following:

HILTI, INC. 7250 DALLAS PARKWAY, SUITE 1000 PLANO, TEXAS 75024 (800) 879-8000 www.hilti.com



#### THREADED ROD/REINFORCING BAR

**HIS-N AND HIS-RN INSERTS** 

#### FIGURE 1—INSTALLATION PARAMETERS FOR POST-INSTALLED ADHESIVE ANCHORS

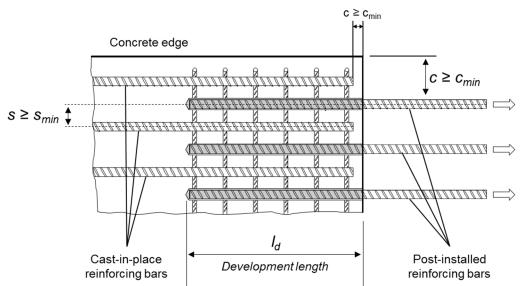


FIGURE 2—INSTALLATION PARAMETERS FOR POST-INSTALLED REINFORCING BARS

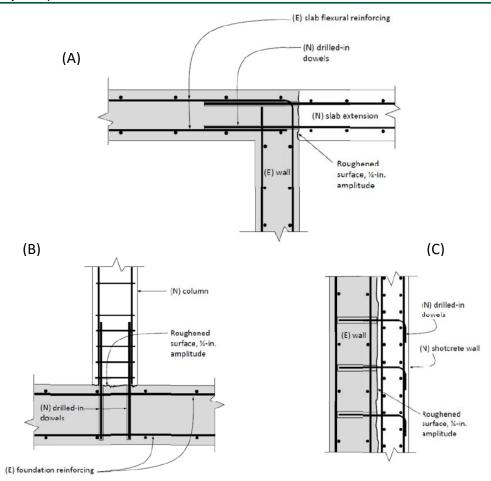
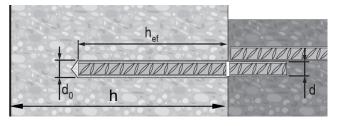


FIGURE 3—(A) TENSION LAP SPLICE WITH EXISTING FLEXURAL REINFORCEMENT; (B) TENSION DEVELOPMENT OF COLUMN DOWELS; (C) DEVELOPMENT OF SHEAR DOWELS FOR NEW ONLAY SHEAR WALL

#### **DEFORMED REINFORCMENT**

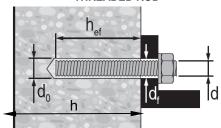


EU Rebar		
Ø d [mm]	Ø d₀ [mm]	h <sub>el</sub> [mm]
8	12	60480
10	14	60600
12	16	70720
14	18	75840
16	20	80960
18	22	851080
20	25	901200
22	28	951320
24	32	961440
25	32	1001500
26	35	1041560
28	35	1121680
30	37	1201800
32	40	1281920

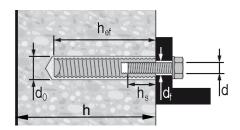
US Rebar		
	Ø d₀	h <sub>ef</sub>
d	[inch]	[inch]
#3	1/2	23/8221/2
#4	5/8	23/430
#5	3/4	3 1/837 1/2
#6	7/8	31/215
# 0	1	1545
#7	1	3 1/217 1/2
# /	1 1/8	17 1/252 1/2
#8	1 1/8	420
# 0	1 1/4	2060
#9	13/8	41/2671/2
#10	1 1/2	575
# 11	13/4	5 1/282 1/2

CA Rebar		
ממממממט	Ø d₀	h <sub>ef</sub>
d	[inch]	[mm]
10 M	9/16	70678
15 M	3/4	80960
20 M	1	901170
25 M	1 1/4 (32 mm)	1011512
30 M	11/2	1201794

#### THREADED ROD



#### HILTI HIS-N AND HIS-RN THREADED INSERTS



HAS / HIT-V

Ø d [inch]	Ø d₀ [inch]	h <sub>ef</sub> [inch]	Ø d <sub>f</sub> [inch]	T <sub>max</sub> [ft-lb]	T <sub>max</sub> [Nm]
3/8	7/16	23/871/2	7/16	15	20
1/2	9/16	23/410	9/16	30	41
5/8	3/4	31/8 121/2	11/16	60	81
3/4	7/8	31/215	<sup>13</sup> / <sub>16</sub>	100	136
7/8	1	31/2 171/2	<sup>15</sup> / <sub>16</sub>	125	169
1	1 1/8	420	1 1/8	150	203
1 1/4	1 3/8	5 25	1 3/8	200	271

mmmmm [m	Ø d <sub>0</sub>	h <sub>ef</sub>	Ø d <sub>f</sub>	T <sub>max</sub>
Ø d [mm]	[mm]	[mm]	[mm]	[Nm]
M8	10	60160	9	10
M10	12	60200	12	20
M12	14	70240	14	40
M16	18	80320	18	80
M20	22	90400	22	150
M24	28	100480	26	200
M27	30	110540	30	270
M30	35	120600	33	300

	Ø d <sub>0</sub>	h <sub>ef</sub>	Ø d <sub>f</sub>		$T_{max}$	$T_{max}$
Ø d [inch]	[inch]	[inch]	[inch]	[inch]	[ft-lb]	[Nm]
3/8	11/16	43/8	7/16	3/8 <sup>15</sup> / <sub>16</sub>	15	20
1/2	7/8	5	9/16	1/21 3/16	30	41
5/8	1 1/8	63/4	11/16	5/81 1/2	60	81
3/4	1 1/4	8 1/8	13/16	3/417/8	100	136

Ø d [mm]	Ø d₀ [mm]	h <sub>ef</sub> [mm]	Ø d <sub>f</sub> [mm]	h <sub>s</sub> [mm]	T <sub>max</sub> [Nm]
M8	14	90	9	820	10
M10	18	110	12	1025	20
M12	22	125	14	1230	40
M16	28	170	18	1640	80
M20	32	205	22	2050	150

### FIGURE 4—INSTALLATION PARAMETERS (Continued)

### TABLE 1—DESIGN TABLE INDEX

Decima 7	Fractional		Metric		
Design Table		Table	Page	Table	Page
Standard Threaded Rod	Steel Strength - $N_{sa}$ , $V_{sa}$	6A	13	14	20
	Concrete Breakout - $N_{cb}$ , $N_{cbg}$ , $V_{cb}$ , $V_{cpg}$ , $V_{cpg}$	7	15	15	21
	Bond Strength - Na, Nag	11-13	18-19	19-21	25-26
Hilti HIS-N and HIS-RN Internally Threaded Insert	Steel Strength - N <sub>sa</sub> , V <sub>sa</sub>	26	30	26	30
	Concrete Breakout - $N_{cb}$ , $N_{cbg}$ , $V_{cb}$ , $V_{cpg}$ , $V_{cpg}$	27	31	27	31
	Bond Strength - Na, Nag	28-30	32-33	28-30	32-33

Doctors :	Fahla	Fract	ional	EU N	letric	Canadian	
Design <sup>-</sup>	lable	Table	Page	Table	Page	Table	Page
Steel Reinforcing Bars	6B	14	14	20	22	27	
	Concrete Breakout - $N_{cb}$ , $N_{cbg}$ , $V_{cb}$ , $V_{cpg}$ , $V_{cpg}$	7	15	15	21	23	27
	Bond Strength - Na, Nag	8-10	16-17	16-18	22-24	24-25B	28-29
	Determination of development length for post-installed reinforcing bar connections	31	34	32	34	33	35

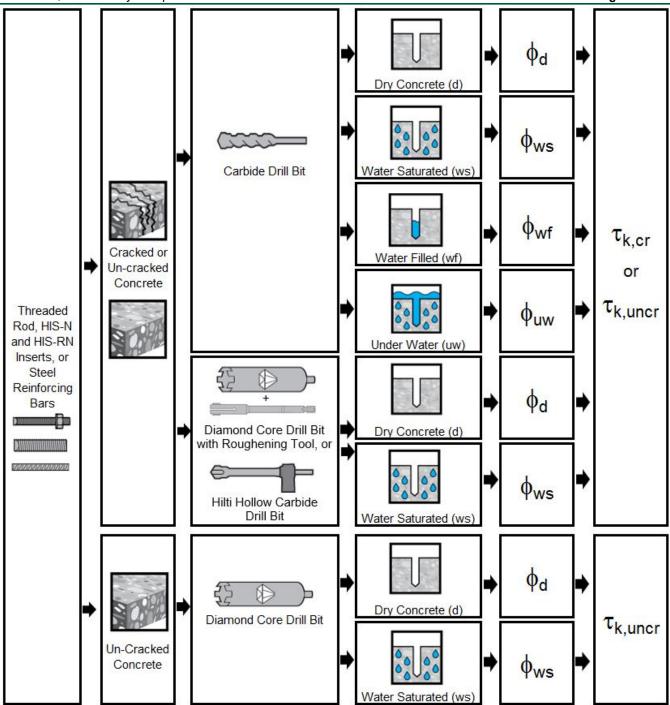


FIGURE 5—FLOWCHART FOR THE ESTABLISHMENT OF DESIGN BOND STRENGTH

#### TABLE 2—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON CARBON AND STAINLESS STEEL THREADED ROD MATERIALS<sup>1</sup>

			1 AND CIAME	SO SIEEL IN			ALU	
THRE	EADED ROD SPECIFICATION	1	Minimum specified ultimate strength, f <sub>uta</sub>	Minimum specified yield strength 0.2 percent offset, $f_{ya}$	f <sub>uta</sub> /f <sub>ya</sub>	Elongation, min. percent <sup>7</sup>	Reduction of Area, min. percent	Specification for nuts <sup>8</sup>
	ASTM A193 <sup>2</sup> Grade B7	psi	125,000	105,000	1.19	16	50	ASTM A563 Grade DH
	≤ 2 <sup>1</sup> / <sub>2</sub> in. (≤ 64 mm)	(MPa)	(862)	(724)	1.19	10	30	ASTIVI ASOS GIAGE DIT
	ASTM F568M³ Class 5.8	psi	72,500	58,000				ASTM A563 Grade DH9
	M5 (¹/₄ in.) to M24 (1 in.) (equivalent to ISO 898-1)	(MPa)	(500)	(400)	1.25	10	35	DIN 934 (8-A2K)
ی	ASTM F1554, Grade 36 <sup>7</sup>	psi	58,000	36,000	1.61	23	40	ASTM A194 or ASTM A563
STEEL	ASTIVIT 1334, Grade 30	(MPa)	(400)	(248)	1.01	23	40	ASTRIA 194 OF ASTRIA 300
S	ASTM F1554, Grade 55 <sup>7</sup>	psi	75,000	55,000	1.36	21	30	ASTM A194 or ASTM A563
CARBON	ASTIVIT 1334, Grade 33	(MPa)	(517)	(379)	1.50	21	30	ASTRIA 194 OF ASTRIA 300
S	ASTM F1554, Grade 105 <sup>7</sup>	psi	125,000	105,000	1.19	15	45	ASTM A194 or ASTM A563
	ASTIVIT 1334, Grade 103	(MPa)	(862)	(724)	1.19	13	40	ASTRIA 194 OF ASTRIA 303
	ISO 898-1 <sup>4</sup> Class 5.8	MPa	500	400	1.25	22		DIN 934 Grade 6
	130 030-1 Class 3.0	(psi)	(72,500)	(58,000)	1.25	22	-	DIN 954 Grade 0
	ISO 898-1 <sup>4</sup> Class 8.8	MPa	800	640	1.25	12	52	DIN 934 Grade 8
	130 090-1 Class 0.0	(psi)	(116,000)	(92,800)	1.25	12	32	DIN 934 Grade 0
	ASTM F593 <sup>5</sup> CW1 (316)	psi	100,000	65,000	1.54	20		ASTM F594
	<sup>1</sup> / <sub>4</sub> -in. to <sup>5</sup> / <sub>8</sub> -in.	(MPa)	(689)	(448)	1.54	20	-	A31W11394
	ASTM F593 <sup>5</sup> CW2 (316)	psi	85,000	45,000	1.89	25		ASTM F594
STEEL	<sup>3</sup> / <sub>4</sub> -in. to 1 <sup>1</sup> / <sub>2</sub> -in.	(MPa)	(586)	(310)	1.09	25	-	A31W11394
SS 8	ASTM A193 Grade 8(M), Class	psi	75,000	30,000	2.50	30	50	ASTM F594
STAINLESS	1 <sup>2</sup> - 1 ¼-in.	(MPa)	(517)	(207)	2.00	30	30	AOTIVIT 394
TAI	ISO 3506-1 <sup>6</sup> A4-70	MPa	700	450	1.56	40	_	ISO 4032
S	M8 – M24	(psi)	(101,500)	(65,250)	1.00	40	_	100 1002
	ISO 3506-1 <sup>6</sup> A4-50	MPa	500	210	2.38	40	_	ISO 4032
	M27 – M30	(psi)	(72,500)	(30,450)	2.50	40	_	100 1002

<sup>1</sup>Hilti HIT-RE 500 V3 adhesive may be used in conjunction with all grades of continuously threaded carbon or stainless steel rod (all-thread) that comply with the code reference standards and that have thread characteristics comparable with ANSI B1.1 UNC Coarse Thread Series or ANSI B1.13M M Profile Metric Thread Series. Values for threaded rod types and associated nuts supplied by Hilti are provided here.

TABLE 3—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON STEEL REINFORCING BARS

REINFORCING BAR SPECIFICATION		Minimum specified ultimate strength, $f_{uta}$	Minimum specified yield strength, $f_{ya}$
ASTM A615 <sup>1</sup> Gr. 60	psi	80,000	60,000
ASTM A015 GI. 00	(MPa)	(550)	(414)
ACTM AC451 C: 40	psi	60,000	40,000
ASTM A615 <sup>1</sup> Gr. 40	(MPa)	(414)	(276)
ASTM A706 <sup>2</sup> Gr. 60	psi	80,000	60,000
ASTM A700- Gr. 60	(MPa)	(550)	(414)
DIN 4003 DOL 500	MPa	550	500
DIN 488 <sup>3</sup> BSt 500	(psi)	(79,750)	(72,500)
OANUOGA GOO 404 O., 400	MPa	540	400
CAN/CSA-G30.18 <sup>4</sup> Gr. 400	(psi)	(78,300)	(58,000)

Standard Specification for Deformed and Plain Carbon Steel Bars for Concrete Reinforcement

<sup>&</sup>lt;sup>2</sup>Standard Specification for Alloy-Steel and Stainless Steel Bolting Materials for High-Temperature Service

<sup>&</sup>lt;sup>3</sup>Standard Specification for Carbon and Alloy Steel Externally Threaded Metric Fasteners

<sup>4</sup>Mechanical properties of fasteners made of carbon steel and alloy steel – Part 1: Bolts, screws and studs

Standard Specification for Stainless Steel Bolts, Hex Cap Screws, and Studs

Mechanical properties of corrosion-resistant stainless steel fasteners – Part 1: Bolts, screws and studs

Mechanical properties of corrosion-resistant stainless steel fasteners – Part 1: Bolts, screws and studs

Based on 2-in. (50 mm) gauge length except for A 193, which are based on a gauge length of 4d and ISO 898, which is based on 5d.

BNuts of other grades and styles having specified proof load stresses greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.

<sup>&</sup>lt;sup>9</sup>Nuts for fractional rods.

<sup>&</sup>lt;sup>2</sup>Standard Specification for Low Alloy Steel Deformed and Plain Bars for Concrete Reinforcement

<sup>&</sup>lt;sup>3</sup>Reinforcing steel; reinforcing steel bars; dimensions and masses

<sup>&</sup>lt;sup>4</sup>Billet-Steel Bars for Concrete Reinforcement

#### TABLE 4—SPECIFICATIONS AND PHYSICAL PROPERTIES OF FRACTIONAL AND METRIC HIS-N AND HIS-RN INSERTS

HILTI HIS-N AND HIS-RN INSERTS		Minimum specified ultimate strength, $f_{uta}$	Minimum specified yield strength, $f_{ya}$
Carbon Steel	psi	71,050	56,550
DIN EN 10277-3 11SMnPb30+c or DIN 1561 9SMnPb28K	(MPa)	(490)	(390)
Stainless Steel	psi	101,500	50,750
EN 10088-3 X5CrNiMo 17-12-2	(MPa)	(700)	(350)

## TABLE 5—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON BOLTS, CAP SCREWS AND STUDS FOR USE WITH HIS-N AND HIS-RN INSERTS<sup>1,2</sup>

BOLT, CAP SCREW OR STUD SPECIFICATION		Minimum specified ultimate strength f <sub>uta</sub>	Minimum specified yield strength 0.2 percent offset $f_{ya}$	f <sub>uta</sub> /f <sub>ya</sub>	Elongation, min.	Reduction of Area, min.	Specification for nuts <sup>6</sup>	
ASTM A193 Grade B7	psi	125,000	105,000	1.119	16	50	ASTM A563 Grade DH	
	(MPa)	(862)	(724)	1.119	10	30	ASTIM ASSO GIAGE DIT	
SAE J429 <sup>3</sup> Grade 5	psi	120,000	92,000	1.30	14	35	SAE J995	
	(MPa)	(828)	(634)	1.50	14	33	OAL 1990	
ASTM A325 <sup>4</sup> 1/ <sub>2</sub> to 1-in.	psi	120,000	92,000	1.30	14	35	A563 C, C3, D, DH, DH3	
AS TIVI AS2S /2 to 1-III.	(MPa)	(828)	(634)	1.30	14	33	Heavy Hex	
ASTM A193 <sup>5</sup> Grade B8M (AISI	psi	110,000	95,000	1.16	15	45	ASTM F594 <sup>7</sup>	
316) for use with HIS-RN	(MPa)	(759)	(655)	1.10	15	45	Alloy Group 1, 2 or 3	
ASTM A193 <sup>5</sup> Grade B8T (AISI	psi	125,000	100,000	1.25	12	35	ASTM F594 <sup>7</sup>	
321) for use with HIS-RN	(MPa)	(862)	(690)	1.25	12	35	Alloy Group 1, 2 or 3	

 $<sup>^{1}\</sup>mbox{Minimum}$  Grade 5 bolts, cap screws or studs must be used with carbon steel HIS inserts.

 $<sup>^2\!</sup>$  Only stainless steel bolts, cap screws or studs must be used with HIS-RN inserts.

<sup>&</sup>lt;sup>3</sup>Mechanical and Material Requirements for Externally Threaded Fasteners

<sup>&</sup>lt;sup>4</sup>Standard Specification for Structural Bolts, Steel, Heat Treated, 120/105 ksi Minimum Tensile Strength

<sup>&</sup>lt;sup>5</sup>Standard Specification for Alloy-Steel and Stainless Steel Bolting Materials for High-Temperature Service

<sup>6</sup>Nuts must have specified minimum proof load stress equal to or greater than the specified minimum full-size tensile strength of the specified stud.

<sup>&</sup>lt;sup>7</sup>Nuts for stainless steel studs must be of the same alloy group as the specified bolt, cap screw, or stud.



#### Fractional Threaded Rod

#### Steel Strength

#### TABLE 6A—STEEL DESIGN INFORMATION FOR FRACTIONAL THREADED ROD

DESIGN	NFORMATION	Symbol	Units			Nomin	al rod diamet	er (in.)¹						
DESIGN	NICKWATION	Syllibol	Ullits	<sup>3</sup> / <sub>8</sub>	1/2	<sup>5</sup> / <sub>8</sub>	3/4	<sup>7</sup> / <sub>8</sub>	1	1 <sup>1</sup> / <sub>4</sub>				
Rod O.D.		d	in.	0.375	0.5	0.625	0.75	0.875	1	1.25				
Rod O.D.		u	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(31.8)				
Pod offor	tive cross-sectional area	A <sub>se</sub>	in. <sup>2</sup>	0.0775	0.1419	0.2260	0.3345	0.4617	0.6057	0.9691				
Rou ellec	live cross-sectional area	Ase	(mm <sup>2</sup> )	(50)	(92)	(146)	(216)	(298)	(391)	(625)				
		N/	lb	5,620	10,290	16,385	24,250	33,470	43,910	70,260				
_	Nominal strength as governed by steel	N <sub>sa</sub>	(kN)	(25.0)	(45.8)	(72.9)	(107.9)	(148.9)	(195.3)	(312.5)				
8-1 5.8	strength		lb	3,370	6,175	9,830	14,550	20,085	26,345	42,155				
88 88		V <sub>sa</sub>	(kN)	(15.0)	(27.5)	(43.7)	(64.7)	(89.3)	(117.2)	(187.5)				
ISO 898-1 Class 5.8	Reduction for seismic shear	αv,seis	-			•	1.0							
<u>∞</u> ∪	Strength reduction factor $\phi$ for tension <sup>2</sup>	φ	-				0.65							
	Strength reduction factor $\phi$ for shear <sup>2</sup>	φ	-				0.60							
-	,	,	lb	9,685	17,735	28,250	41,810	57,710	75,710	121,135				
B7	Nominal strength as governed by steel	N <sub>sa</sub>	(kN)	(43.1)	(78.9)	(125.7)	(186.0)	(256.7)	(336.8)	(538.8)				
93	strength		lb	5,810	10,640	16,950	25,085	34,625	45,425	72,680				
ξ		V <sub>sa</sub>	(kN)	(25.9)	(47.3)	(75.4)	(111.6)	(154.0)	(202.1)	(323.3)				
ASTM A193 B7	Reduction for seismic shear	αv,seis	-	(====)	()	(1.51.1)	1.0	(,	(===::/	(====)				
ST	Strength reduction factor $\phi$ for tension <sup>3</sup>	φ	-				0.75							
∢	Strength reduction factor $\phi$ for shear <sup>3</sup>	φ	-				0.65							
	Changar reduction factor & for oriotal	-	lb	-	8.230	13,110	19.400	26,780	35,130	56,210				
. <b>4</b>	Nominal strength as governed by steel	N <sub>sa</sub>	(kN)	_	(36.6)	(58.3)	(86.3)	(119.1)	(156.3)	(250.0)				
9	strength	.,	lb	-	4,940	7,865	11,640	16,070	21,080	33,725				
μõ	3	V <sub>sa</sub>	(kN)	-	(22.0)	(35.0)	(51.8)	(71.5)	(93.8)	(150.0)				
≥ຼັບັ	Reduction factor, seismic shear	$\alpha_{v,seis}$	-	0.6										
ASTM F1554 Gr. 36	Strength reduction factor $\phi$ for tension <sup>3</sup>	φ	-	0.75										
,	Strength reduction factor $\phi$ for shear <sup>3</sup>	φ	-				0.65							
	Nominal strength as governed by steel	A.	lb	-	10,645	16,950	25,090	34,630	45,430	72,685				
4		N <sub>sa</sub>	(kN)	-	(47.4)	(75.4)	(111.6)	(154.0)	(202.1)	(323.3)				
F15£	strength	V <sub>sa</sub>	lb	-	6,385	10,170	15,055	20,780	27,260	43,610				
7 F		<b>V</b> sa	(kN)	-	(28.4)	(45.2)	(67.0)	(92.4)	(121.3)	(194.0)				
ASTM F1554 Gr. 55	Reduction factor, seismic shear	αv,seis	-				1.0							
AS	Strength reduction factor $\phi$ for tension <sup>3</sup>	$\phi$	-				0.75							
	Strength reduction factor $\phi$ for shear <sup>3</sup>	$\phi$	-				0.65							
		N <sub>sa</sub>	lb	-	17,740	28,250	41,815	57,715	75,715	121,135				
72	Nominal strength as governed by steel	IVsa	(kN)	-	(78.9)	(125.7)	(186.0)	(256.7)	(336.8)	(538.8)				
15	strength	V <sub>sa</sub>	lb	-	10,645	16,950	25,090	34,630	45,430	72,680				
2 ·		v sa	(kN)	-	(47.4)	(75.4)	(111.6)	(154.0)	(202.1)	(323.3)				
ASTM F1554 Gr. 105	Reduction factor, seismic shear	αv,seis	-				1.0							
š	Strength reduction factor $\phi$ for tension <sup>3</sup>	φ	-				0.75							
	Strength reduction factor $\phi$ for shear <sup>3</sup>	φ	-		T		0.65							
≥		N <sub>sa</sub>	lb	7,750	14,190	22,600	28,435	39,245	51,485	-				
o, °	Nominal strength as governed by steel	- 100	(kN)	(34.5)	(63.1)	(100.5)	(126.5)	(174.6)	(229.0)	-				
93 es	strength	$V_{sa}$	lb (LN)	4,650	8,515	13,560	17,060	23,545	30,890	-				
ASTM F593, CW Stainless	Deduction feature actions above		(kN)	(20.7)	(37.9)	(60.3)	(75.9)	(104.7)	(137.4)	-				
<u>≅</u> ౘ	Reduction factor, seismic shear	αν,seis	-				.80			-				
S	Strength reduction factor $\phi$ for tension <sup>2</sup>	φ	-				.65			-				
	Strength reduction factor $\phi$ for shear <sup>2</sup>	φ	- 11-				.60			-				
نے	Name and the same	Nsa	lb (kN)				-			55,240				
s 4.	Nominal strength as governed by steel		(kN) Ib							(245.7) 33,145				
las les	strength	V <sub>sa</sub>	(kN)											
₹ό≝	Paduation factor, aciamia chase		. ,				_			0.8				
St()	Reduction factor, seismic shear  Strength reduction factor $\phi$ for tension <sup>2</sup>	αν,seis ₁	-				<u>-</u>			0.8				
ASTM A193, Gr. 8(M), Class 1 Stainless		φ	-											
-	Strength reduction factor $\phi$ for shear <sup>2</sup>	$\phi$	-				-			0.65				

For **SI**: 1 inch = 25.4 mm, 1 lbf = 4.448 N. For **pound-inch** units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf

¹Values provided for common rod material types are based on specified strengths and calculated in accordance with ACI 318-19 Eq. (17.6.1.2) and Eq. (17.7.1.2b), ACI 318-14 Eq. (17.4.1.2) and Eq (17.5.1.2b) or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must be appropriate for the rod. ²For use with the load combinations of Section 1605.1 of the 2021 IBC or Section 1605.2 of the 2018, 2015, and 2012 IBC, ACI 318 (-19 and -14) 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3 or ACI 318-14 17.3.3 or ACI 318-11 D.4.4. Values correspond to a brittle steel element. ³For use with the load combinations of Section 1605.1 of the 2021 IBC or Section 1605.2 of the 2018, 2015, and 2012 IBC, ACI 318 (-19 and -14) 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3 or ACI 318-14 17.3.3 or ACI 318-11 D.4.4. values correspond to a brittle steel element.

used, the appropriate value of  $\phi$  must be determined in accordance with ACI 318-11 D.4.4. Values correspond to a ductile steel element.





#### **Fractional Reinforcing Bars**

#### Steel Strength

#### TABLE 6B—STEEL DESIGN INFORMATION FOR FRACTIONAL REINFORCING BARS

DEGICI	LINEODMATION	Oh al	1114			Nomina	l Reinforcii	ng bar size	(Rebar) <sup>1</sup>			
DESIGI	NINFORMATION	Symbol	Units	#3	#4	#5	#6	#7	#8	#9	#10	
Ni	h di		in.	3/8	1/2	5/8	3/4	7/8	1	1.128	1.270	
inomina	I bar diameter	d	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(28.7)	(32.3)	
Day offer	ctive cross-sectional area	4	in. <sup>2</sup>	0.11	0.2	0.31	0.44	0.60	0.79	1.00	1.27	
bai elle	ctive cross-sectional area	Ase	(mm²)	(71)	(129)	(199)	(284)	(387)	(510)	(645)	(819)	
		N <sub>sa</sub>	lb	6,600	12,000	18,600	26,400	36,000	47,400	60,000	76,200	
	Nominal strength as governed by steel		(kN)	(29.4)	(53.4)	(82.7)	(117.4)	(160.1)	(210.9)	(266.9)	(339.0)	
.615 40	strength		lb	3,960	7,200	11,160	15,840	21,600	28,440	36,000	45,720	
M A ade	Strength Reduction for seismic shear		(kN)	(17.6)	(32.0)	(49.6)	(70.5)	(96.1)	(126.5)	(160.1)	(203.4)	
AST Gr	Reduction for seismic shear	$lpha_{ m V,seis}$	-	0.70								
	Strength reduction factor $\phi$ for tension <sup>2</sup>	φ	-				0.	65				
	Strength reduction factor $\phi$ for shear $^2$	φ	-		0.60							
		Α.	lb	8,800	16,000	24,800	35,200	48,000	63,200	80,000	101,600	
	Nominal strength as governed by steel	N <sub>sa</sub>	(kN)	(39.1)	(71.2)	(110.3)	(156.6)	(213.5)	(281.1)	(355.9)	(451.9)	
615 60	strength	V <sub>sa</sub>	lb	5,280	9,600	14,880	21,120	28,800	37,920	48,000	60,960	
STM A61 Grade 60		V sa	(kN)	(23.5)	(42.7)	(66.2)	(93.9)	(128.1)	(168.7)	(213.5)	(271.2)	
ASTM A615 Grade 60	Reduction for seismic shear	αv,seis	-				0.	70				
	Strength reduction factor $\phi$ for tension <sup>2</sup>	φ	-				0.	65				
	Strength reduction factor $\phi$ for shear <sup>2</sup>	φ	-				0.	60				
		.,	lb	8,800	16,000	24,800	35,200	48,000	63,200	80,000	101,600	
	Nominal strength as governed by steel	N <sub>sa</sub>	(kN)	(39.1)	(71.2)	(110.3)	(156.6)	(213.5)	(281.1)	(355.9)	(452.0)	
706 60	strength		lb	5,280	9,600	14,880	21,120	28,800	37,920	48,000	60,960	
STM A70		V <sub>sa</sub>	(kN)	(23.5)	(42.7)	(66.2)	(94.0)	(128.1)	(168.7)	(213.5)	(271.2)	
ASTM A706 Grade 60	Reduction for seismic shear	αv,seis					0.	70				
`	Strength reduction factor $\phi$ for tension <sup>3</sup>	φ					0.	75				
	Strength reduction factor $\phi$ for shear <sup>3</sup>	φ		0.65								

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf

<sup>&</sup>lt;sup>1</sup> Values provided for common rebar types are based on specified strengths and calculated in accordance with ACI 318-19 Eq. (17.6.1.2) and Eq. (17.7.1.2b), ACI 318-14 Eq. (17.4.1.2) and Eq. (17.5.1.2b) or ACI 318-14 Eq. (D-2) Nuts and washers must be appropriate for the rod

<sup>318-14</sup> Eq. (17.4.1.2) and Eq (17.5.1.2b) or ACI 318-11 Eq. (D-2) and Eq. (D-29). Nuts and washers must be appropriate for the rod.

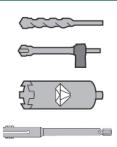
For use with the load combinations of Section 1605.1 of the 2021 IBC or Section 1605.2 of the 2018, 2015, and 2012 IBC, ACI 318 (-19 and -14) 5.3 or ACI 318-11 9.2, as set forth in ACI 318-19 17.5.3 or ACI 318-14 17.3.3 or ACI 318-11 D.4.3. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of φ must be determined in accordance with ACI 318-11 D.4.4. Values correspond to a brittle steel element.

³ For use with the load combinations of Section 1605.1 of the 2021 IBC or Section 1605.2 of the 2018, 2015, and 2012 IBC, ACI 318 (-19 and -14) 5.3 or ACI 318-11 9.2, as set forth in ACI 318-19 17.5.3 or ACI 318-14 17.3.3 or ACI 318-11 D.4.3. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of *ϕ* must be determined in accordance with ACI 318-11 D.4.4. Values correspond to a ductile steel element.









Carbide Bit or Hilti Hollow Carbide Bit Diamond Core Bit + Roughening Tool, or Diamond Core Bit

#### TABLE 7—CONCRETE BREAKOUT DESIGN INFORMATION FOR FRACTIONAL THREADED ROD AND REINFORCING BARS ALL DRILLING METHODS<sup>1</sup>

						Nomina	l rod dia	meter (i	n.) / Reir	nforcing	bar size			
DESIGN INFORMATION	Symbol	Units	<sup>3</sup> / <sub>8</sub> or #3	1/2	#4	<sup>5</sup> / <sub>8</sub>	#5	3/4	#6	7/8	#7	1 or #8	#9	1 <sup>1</sup> / <sub>4</sub> or #10
Effectiveness factor for	le.	in-lb			•		•	1	7	•				•
cracked concrete	K <sub>c,cr</sub>	(SI)						(7	.1)					
Effectiveness factor for	k <sub>c.uncr</sub>	in-lb						2	4					
uncracked concrete	<b>∧</b> c,uncr	(SI)						(1	0)					
Minimum Embedment	h <sub>ef.min</sub>	in.	23/8	$2^{3}/_{4}$	2 <sup>3</sup> / <sub>8</sub>	31/8	3	31/2	3	31/2	33/8	4	41/2	5
	Tier,min	(mm)	(60)	(70)	(60)	(79)	(76)	(89)	(76)	(89)	(85)	(102)	(114)	(127)
Maximum Embedment	h .	in.	71/2	10	10	12 <sup>1</sup> / <sub>2</sub>	12 <sup>1</sup> / <sub>2</sub>	15	15	17 <sup>1</sup> / <sub>2</sub>	17 <sup>1</sup> / <sub>2</sub>	20	221/2	25
waximum Embedment	h <sub>ef,max</sub>	(mm)	(191)	(254)	(254)	(318)	(318)	(381)	(381)	(445)	(445)	(508)	(572)	(635)
Min. anchor spacing <sup>3</sup>	pacing <sup>3</sup> s <sub>min</sub>	in.	1 <sup>7</sup> / <sub>8</sub>	21/2	21/2	3 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>8</sub>	33/4	33/4	43/8	43/8	5	5 <sup>5</sup> / <sub>8</sub>	6 <sup>1</sup> / <sub>4</sub>
wiiii. aliciloi spacilig		(mm)	(48)	(64)	(64)	(79)	(79)	(95)	(95)	(111)	(111)	(127)	(143)	(159)
Min. edge distance <sup>3</sup>	Cmin	-	5	id; or se	e Sectior	1 4.1.9 of	this rep	ort for de	sign with	reduce	d minimu	m edge	distance	:S
Minimum concrete	h <sub>min</sub>	in.		h <sub>ef</sub> + 1 <sup>1</sup> /	4					h <sub>ef</sub> + 2d <sub>0</sub>	(4)			
thickness	***************************************	(mm)		$(h_{ef} + 30)$	))					riei · Zuo				
Critical edge distance – splitting (for uncracked concrete)	Cac	-					See See	ction 4.1	10 of this	s report.				
Strength reduction factor for tension, concrete failure modes <sup>2</sup>	φ	1						0.	65					
Strength reduction factor for shear, concrete failure modes <sup>2</sup>	φ	-						0.	70					

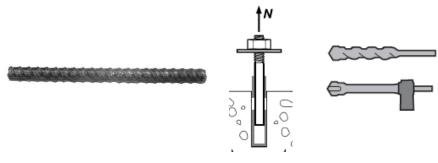
For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 8A and 8B, Manufacturers Printed Installation Instructions (MPII).

<sup>&</sup>lt;sup>2</sup>The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, the appropriate strength reduction factor must be determined in accordance with ACI 318-11 D.4.4.

<sup>3</sup>For installations with 1<sup>3</sup>/<sub>4</sub>-inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

 $<sup>^4</sup>d_0$  = hole diameter.



**Fractional Reinforcing Bars** 

**Bond Strength** 

Carbide Bit or Hilti Hollow Carbide Bit

TABLE 8—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT)1

		<b></b>			·		No	minal reinfo	orcing bar	size		
DESIG	IN INFO	DRMATION	Symbol	Units	#3	#4	#5	#6	#7	#8	#9	#10
Minimu	ım Emk	pedment	h	in.	2 <sup>3</sup> / <sub>8</sub>	2 <sup>3</sup> / <sub>8</sub>	3	3	33/8	4	41/2	5
IVIIIIIIII	1111 E111K	beament	h <sub>ef,min</sub>	(mm)	(60)	(60)	(76)	(76)	(85)	(102)	(114)	(127)
Maxim	um Em	bedment	h	in.	7½	10	12½	15	17½	20	22½	25
IVIAXIIII	ulli Elli	pedifient	h <sub>ef,max</sub>	(mm)	(191)	(254)	(318)	(381)	(445)	(508)	(572)	(635)
- D	<u>e</u>	Characteristic bond strength in	_	psi	1,350	1,360	1,390	1,410	1,410	1,420	1,390	1,340
ırate	ratt e A	cracked concrete	Tk,cr	(MPa)	(9.3)	(9.4)	(9.6)	(9.7)	(9.7)	(9.8)	(9.6)	(9.3)
Dry concrete and Water Saturated Concrete	emperature range A²	Characteristic bond strength in	_	psi	1,770	1,740	1,720	1,690	1,670	1,640	1,620	1,590
e ter	E -	uncracked concrete	Tk,uncr	(MPa)	(12.2)	(12.0)	(11.9)	(11.7)	(11.5)	(11.3)	(11.2)	(11.0)
Wa	<u>e</u>	Characteristic bond strength in	_	psi	930	940	960	970	980	980	960	930
and Wat Concrete	emperature range B <sup>2</sup>	cracked concrete	Tk,cr	(MPa)	(6.4)	(6.5)	(6.6)	(6.7)	(6.7)	(6.8)	(6.6)	(6.4)
ete	mpe	Characteristic bond strength in		psi	1,220	1,200	1,190	1,170	1,150	1,130	1,120	1,100
nc	ชื่อ uncracked concrete		T <sub>k,uncr</sub>	(MPa)	(8.4)	(8.3)	(8.2)	(8.1)	(7.9)	(7.8)	(7.7)	(7.6)
გ გ	Anchor Category		-	-	1	1	1	1	1	1	1	1
۵	Stren	th Reduction factor	φ <sub>d</sub> , φ <sub>ws</sub>	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	i.e	Characteristic bond strength in	-	psi	1,000	1,010	1,040	1,060	1,070	1,090	1,070	1,050
	eratu e A	cracked concrete	Tk,cr	(MPa)	(6.9)	(6.9)	(7.2)	(7.3)	(7.4)	(7.5)	(7.4)	(7.2)
40	Temperature range A <sup>2</sup>	Characteristic bond strength in	Tk,uncr	psi	1,300	1,290	1,290	1,280	1,270	1,260	1,240	1,240
Water-filled hole	Je _	uncracked concrete		(MPa)	(9.0)	(8.9)	(8.9)	(8.8)	(8.7)	(8.7)	(8.6)	(8.6)
<u>9</u>	<u>e</u> <u></u>	Characteristic bond strength in		psi	690	700	720	730	740	750	740	720
il-i	emperature range B²	cracked concrete	Tk,cr	(MPa)	(4.7)	(4.8)	(5.0)	(5.0)	(5.1)	(5.2)	(5.1)	(5.0)
Vate	empera range	Characteristic bond strength in	_	psi	900	890	890	880	870	870	860	860
>	E _	uncracked concrete	Tk,uncr	(MPa)	(6.2)	(6.1)	(6.1)	(6.1)	(6.0)	(6.0)	(5.9)	(5.9)
	Ancho	or Category	-	-	3	3	3	3	3	3	3	3
	Stren	gth Reduction factor	$\phi_{wf}$	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
	ıre 2	Characteristic bond strength in	7.	psi	860	890	920	940	960	990	970	980
	e A	cracked concrete	T <sub>k,cr</sub>	(MPa)	(5.9)	(6.1)	(6.3)	(6.5)	(6.6)	(6.9)	(6.7)	(6.8)
ete	Temperature range A <sup>2</sup>	Characteristic bond strength in	_	psi	1,140	1,130	1,140	1,140	1,140	1,150	1,130	1,150
ncre	Je J	uncracked concrete	T <sub>k,uncr</sub>	(MPa)	(7.9)	(7.8)	(7.9)	(7.9)	(7.9)	(7.9)	(7.8)	(8.0)
8	e	Characteristic bond strength in	-	psi	590	610	630	650	660	690	670	680
<u>ī</u> ge	eratu e B²	cracked concrete	Tk,cr	(MPa)	(4.1)	(4.2)	(4.4)	(4.5)	(4.6)	(4.7)	(4.6)	(4.7)
ome	emperature range B <sup>2</sup>	Characteristic bond strength in	7.	psi	790	780	790	790	790	790	790	800
Submerged concrete	Te.	uncracked concrete	Tk,uncr	(MPa)	(5.4)	(5.4)	(5.4)	(5.4)	(5.4)	(5.5)	(5.4)	(5.5)
	Ancho	r Category	-	-	3	3	3	3	3	3	3	3
	Strength Reduction factor		$\phi_{\sf uw}$	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduc	tion for	seismic tension	α <sub>N,seis</sub>	-	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

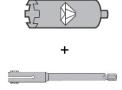
Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c / 2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c / 17.2)^{0.25}$ ] and  $(f_c / 2,500)^{0.15}$  for cracked concrete [For SI:  $(f_c / 17.2)^{0.15}$ ]. See Section 4.1.4 of this report for bond strength determination. <sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







**Fractional Reinforcing Bars** 

**Bond Strength** 

Diamond Core Bit + **Roughening Tool** 

#### TABLE 9—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL REINFORCING BARS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL<sup>1</sup>

DECIONII	NEODMATION		0	l laita		Nomin	al reinforcing	bar size	
DESIGN II	NFORMATION		Symbol	Units	#5	#6	#7	#8	#9
Minimum I	Embedment		6	in.	3	3	33/8	4	41/2
iviiriimum E	Embeament		h <sub>ef,min</sub>	(mm)	(76)	(76)	(85)	(102)	(115)
Maximum	Embedment		h <sub>ef.max</sub>	in.	121/2	11 1/4	17½	20	221/2
IVIAXIIIIUIII	Linbedinent		I let,max	(mm)	(318)	(286)	(445)	(508)	(573)
क	Temperature range A <sup>2</sup> Characteristic bond strength in cracked concrete  Characteristic bond strength		Tk.cr	psi	970	990	990	995	970
ICre	Temperature		ık,cr	(MPa)	(6.7)	(6.8)	(6.8)	(6.9)	(6.7)
	range A <sup>2</sup>	Characteristic bond strength in uncracked concrete	T <sub>k.uncr</sub>	psi	1,720	1,690	1,670	1,640	1,620
atec			r,unci	(MPa)	(11.9)	(11.7)	(11.5)	(11.3)	(11.2)
saturated		Characteristic bond strength	Tk.cr	psi	670	680	680	690	670
	Temperature	in cracked concrete	UK,CI	(MPa)	(4.6)	(4.7)	(4.7)	(4.8)	(4.6)
and water	range B <sup>2</sup>	Characteristic bond strength	Tk.uncr	psi	1,190	1,170	1,150	1,130	1,120
anc		in uncracked concrete	en,uno	(MPa)	(8.2)	(8.1)	(7.9)	(7.8)	(7.7)
Dry	Anchor Categor	у	-	-	1	1	1	1	1
	Strength Reduc	tion factor	$\phi_{d},\phi_{ws}$	-	0.65	0.65	0.65	0.65	0.65
Reduction	luction for seismic tension			-	0.9	0.9	0.9	0.9	0.9

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-incir utilis. I fill = 0.0393/ illicites, 1 N = 0.2246 ibi, 1 NF a = 143.0 psi

Bond strength values correspond to concrete compressive strength in the range 2,500 psi ≤ f'c ≤ 8,000 psi).

Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







Fractional Reinforcing Bars

**Bond Strength** 

**Diamond Core Bit** 

#### TABLE 10—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL REINFORCING BARS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT1

DEGL	NUNECODMATION		Oh. a.l	Units			Nomi	nal reinfo	orcing ba	r size		
DESIG	SN INFORMATION		Symbol	Symbol Units		#4	#5	#6	#7	#8	#9	#10
Minim	linimum Embedment		h	in.	23/8	2 <sup>3</sup> / <sub>8</sub>	3	3	33/8	4	41/2	5
IVIIIIIIII	indin Embedment		h <sub>ef,min</sub>	(mm)	(60)	(60)	(76)	(76)	(85)	(102)	(114)	(127)
Maxim	kimum Embedment		h.	in.	71/2	10	12½	15	171/2	20	22½	25
IVIANIII			h <sub>ef,max</sub>	(mm)	(191)	(254)	(318)	(381)	(445)	(508)	(572)	(635)
r ete		Characteristic bond strength in	7	psi	1,150	1,150	1,150	1,150	1,150	1,150	1,150	1,150
water	A <sup>2</sup>	uncracked concrete	Tk,uncr	(MPa)	(8.0)	(8.0)	(8.0)	(8.0)	(8.0)	(8.0)	(8.0)	(8.0)
~ ~		Characteristic bond strength in	_	psi	800	800	800	800	800	800	800	800
	B <sup>2</sup> uncracked concrete		Tk,uncr	(MPa)	(5.5)	(5.5)	(5.5)	(5.5)	(5.5)	(5.5)	(5.5)	(5.5)
Dry	Anchor Category		-	-	2	2	3	3	3	3	3	3
	Strength Reduction	Strength Reduction factor			0.55	0.55	0.45	0.45	0.45	0.45	0.45	0.45

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

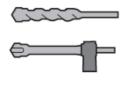
<sup>1</sup>Bond strength values correspond to concrete compressive strength f'<sub>c</sub> = 2,500 psi (17.2 MPa). For concrete compressive strength, f'<sub>c</sub>, between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of (f<sub>c</sub> / 2,500)<sup>0.25</sup> for uncracked concrete. [For SI: (f<sub>c</sub> / All 2) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of (7.2,000). The tabulated characteristic bond strength nine yet increased by a factor of (7.2,000). The tabulated characteristic bond strength nine yet increased by a factor of (7.2,000). The tabulated character is consistent in the properties. It is is the factor of (7.2,000). The tabulated character is consistent in the properties. It is is the factor of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is consistent in the properties of (7.2,000). The tabulated character is co

roughly constant over significant periods of time.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi







Fractional Threaded Rod

**Bond Strength** 

Carbide Bit or Hilti Hollow Carbide Bit

#### TABLE 11—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT)1

	DEC	SIGN INFORMATION	Symbol	Units			Nomin	al rod diar	neter (in.)		
	DES	SIGN INFORMATION	Symbol	Ullits	3/8	1/2	5/8	3/4	<sup>7</sup> / <sub>8</sub>	1	11/4
Minimun	n Embod	lmont	h	in.	23/8	23/4	31/8	31/2	31/2	4	5
Willillian	II EIIIbeu	iment	h <sub>ef,min</sub>	(mm)	(60)	(70)	(79)	(89)	(89)	(102)	(127)
Maximui	m Embe	dment	h <sub>ef.max</sub>	in.	7½	10	12½	15	17½	20	25
IVIAXIIIIUI	III LIIIDE	ument	TTet,max	(mm)	(191)	(254)	(318)	(381)	(445)	(508)	(635)
	ature A²	Characteristic bond strength in	$ au_{\kappa, cr}$	psi	1,280	1,270	1,260	1,250	1,240	1,240	1,180
	Temperature range A <sup>2</sup>	cracked concrete	t K,CI	(MPa)	(8.8)	(8.7)	(8.7)	(8.6)	(8.6)	(8.5)	(8.1)
ater e	empera range /	Characteristic bond strength in	$ au_{\kappa, uncr}$	psi	2,380	2,300	2,210	2,130	2,040	1,960	1,790
y concrete and Wat Saturated Concrete		uncracked concrete	v k,unci	(MPa)	(16.4)	(15.8)	(15.3)	(14.7)	(14.1)	(13.5)	(12.4)
and	Temperature range B <sup>2</sup>	Characteristic bond strength in	$ au_{\kappa, cr}$	psi	880	870	870	860	860	850	810
rete	erati ge B	cracked concrete	t K,Cl	(MPa)	(6.1)	(6.0)	(6.0)	(5.9)	(5.9)	(5.9)	(5.6)
conc	empera range l	Characteristic bond strength in	Т <sub>к</sub> ,uncr	psi	1,640	1,590	1,530	1,470	1,410	1,350	1,240
ory o	<u> </u>		t k,unci	(MPa)	(11.3)	(10.9)	(10.5)	(10.1)	(9.7)	(9.3)	(8.5)
	Anchor Category		-	-	1	1	1	1	1	1	1
	Strength Reduction factor		фа, фws	φδ, φωσ	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	I.e	Characteristic bond strength in		psi	940	940	940	940	940	950	920
	ratur e A²	cracked concrete	$ au_{\kappa, cr}$	(MPa)	(6.5)	(6.5)	(6.5)	(6.5)	(6.5)	(6.5)	(6.4)
_	Temperature range A <sup>2</sup>	Characteristic bond strength in	Τκ,uncr	psi	1,760	1,700	1,660	1,600	1,550	1,500	1,400
Water-filled hole	Te	uncracked concrete		(MPa)	(12.1)	(11.7)	(11.4)	(11.0)	(10.7)	(10.4)	(9.7)
<u>eq</u>	e Ie	Characteristic bond strength in	_	psi	650	650	650	650	650	650	640
er-fi	Temperature range B <sup>2</sup>	cracked concrete	$ au_{\kappa, cr}$	(MPa)	(4.5)	(4.5)	(4.5)	(4.5)	(4.5)	(4.5)	(4.4)
Wat	empera	Characteristic bond strength in	-	psi	1,210	1,170	1,140	1,110	1,070	1,040	970
-	Te	uncracked concrete	$ au_{\kappa, uncr}$	(MPa)	(8.4)	(8.1)	(7.9)	(7.6)	(7.4)	(7.1)	(6.7)
	Anchor	Category	-	-	3	3	3	3	3	3	3
	Strength	Reduction factor	$\Phi_{Wf}$	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45
	, <u>re</u>	Characteristic bond strength in	-	psi	820	830	830	840	850	860	860
	Temperature range A²	cracked concrete	$ au_{\kappa, cr}$	(MPa)	(5.7)	(5.7)	(5.8)	(5.8)	(5.9)	(5.9)	(5.9)
e te	empera range ,	Characteristic bond strength in	T	psi	1,530	1,500	1,470	1,430	1,400	1,370	1,300
ncr	¥ _	uncracked concrete	Тк,uncr	(MPa)	(10.6)	(10.3)	(10.1)	(9.9)	(9.6)	(9.4)	(9.0)
8	2 Le	Characteristic bond strength in	<b>7</b>	psi	570	570	580	580	590	590	590
Submerged concrete	Temperature range B <sup>2</sup>	cracked concrete	$ au_{K,Cr}$	(MPa)	(3.9)	(3.9)	(4.0)	(4.0)	(4.0)	(4.1)	(4.1)
, p	empera range l	Characteristic bond strength in	τ	psi	1,060	1,030	1,010	990	960	940	900
જ	ř	uncracked concrete	$ au_{\kappa, uncr}$	(MPa)	(7.3)	(7.1)	(7.0)	(6.8)	(6.6)	(6.5)	(6.2)
	Anchor	Anchor Category		-	3	3	3	3	3	3	3
	Strength Reduction factor		фим	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction	eduction for seismic tension		CLN,seis	-	0.92	0.93	0.95	1	1	1	1

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c/17.2)^{0.15}$ ]. See Section 4.1.4 of this report for bond strength determination.

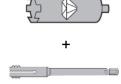
2 Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







**Fractional Threaded Rod** 

**Bond Strength** 

Diamond Core Bit + **Roughening Tool** 

#### TABLE 12—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED RODS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL1

						Nomina	I rod diamet	er (in.)	
DESIG	INFORMATION		Symbol	Units	5/8	3/4	7/8	1	11/4
Minima	ım Embedment		<b>b</b>	in.	31/8	31/2	3½	4	5
IVIIIIIIII	ım Embedmeni		h <sub>ef,min</sub>	(mm)	(79)	(89)	(89)	(102)	(127)
Mavina	um Embedment		6	in.	12½	111/4	17½	20	25
Maxiiii	um Embeament		h <sub>ef,max</sub>	(mm)	(318)	(286)	(445)	(508)	(635)
te		Characteristic bond strength in	_	psi	880	875	870	870	825
cre	Temperature cracked concrete	Tk,cr	(MPa)	(6.1)	(6.0)	(6.0)	(6.0)	(5.7)	
d concrete	range A <sup>2</sup>	Characteristic bond strength in	_	psi	2,210	2,130	2,040	1,960	1,790
ted		uncracked concrete	$ au_{k,uncr}$	(MPa)	(15.3)	(14.7)	(14.1)	(13.5)	(12.4)
saturated		Characteristic bond strength in		psi	610	605	605	600	570
r sa	Temperature	cracked concrete	T <sub>k,cr</sub>	(MPa)	(4.2)	(4.2)	(4.2)	(4.1)	(3.9)
water	range B²	Characteristic bond strength in		psi	1,530	1,470	1,410	1,350	1,240
and v		uncracked concrete	$ au_{k,uncr}$	(MPa)	(10.5)	(10.1)	(9.7)	(9.3)	(8.5)
a <	Anchor Category  Strength Reduction factor		-	-	1	1	1	1	1
ے ۔	Strength Reduction factor			-	0.65	0.65	0.65	0.65	0.65
Reduc	tion for seismic ter	nsion	QN, seis	-	0.95	1	1	1	1

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Bond strength values correspond to concrete compressive strength in the range 2,300 ps > 1.0 > 0,000 ps.

2Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







Fractional Threaded Rod

**Bond Strength** 

**Diamond Core Bit** 

#### TABLE 13—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL THREADED RODS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT1

DESIGN	INFORMATION		Cumbal	Units			Nomin	al rod diame	ter (in.)		
DESIGN	INFORMATION		Symbol	Units	<sup>3</sup> / <sub>8</sub>	1/2	5/8	3/4	<sup>7</sup> / <sub>8</sub>	1	1 1/4
Minimun	n Embedment		h	in.	2 <sup>3</sup> / <sub>8</sub>	23/4	31/8	31/2	31/2	4	5
wiiiiiiiiiiiii	i Embedment		h <sub>ef,min</sub>	(mm)	(60)	(70)	(79)	(89)	(89)	(102)	(127)
Maximus	n Embodmont		h .	in.	7½	10	12½	15	17½	20	25
Maximu	ximum Embedment  Characteristic bond		h <sub>ef,max</sub>	(mm)	(191)	(254)	(318)	(381)	(445)	(508)	(635)
	Temperature	Characteristic bond		psi	1,550	1,550	1,550	1,550	1,550	1,550	1,550
ncrete and saturated ncrete	range A <sup>2</sup> strength in uncracked concrete		Tk,uncr	(MPa)	(10.7)	(10.7)	(10.7)	(10.7)	(10.7)	(10.7)	(10.7)
atur zrete	Temperature	Characteristic bond		psi	1,070	1,070	1,070	1,070	1,070	1,070	1,070
Dry concrete Water satura concrete	range B <sup>2</sup>	strength in uncracked concrete	Tk,uncr	(MPa)	(7.4)	(7.4)	(7.4)	(7.4)	(7.4)	(7.4)	(7.4)
Wa	Anchor Category		-	-	2	2	3	3	3	3	3
	Strength Reduct	ion factor	φ <sub>d</sub> , φ <sub>ws</sub>	-	0.55	0.55	0.45	0.45	0.45	0.45	0.45

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

<sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c/17.2)^{0.25}$ ]. See and 8,000 psi (55.2 MPa), the tabulated dial accerts to boild strength may be increased by a factor of (7.57.2,007) for dial accerts to 50.0 (7.57.17.2), 1.50 Section 4.1.4 of this report for bond strength determination.

2 Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength in the range 2,500 psi ≤ f'c ≤ 8,000 psi.

constant over significant periods of time.





Metric Threaded Rod and EU Metric Reinforcing Bars

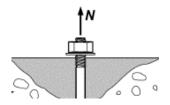
Steel Strength

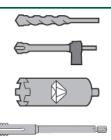
#### TABLE 14—STEEL DESIGN INFORMATION FOR METRIC THREADED ROD AND EU METRIC REINFORCING BARS

	TABLE 14—STEE	DEGIG	V IIVI OI	NIA HOIT	OK WILT	III IIIILA		I rod diame		LINI OKO	ING DAIG		
DESIG	N INFORMATION	Symbol	Units	8	10	12	1		20	24	27	30	
			mm	8	10	12	1		20	24	27	30	
Rod O	utside Diameter	d	(in.)	(0.31)	(0.39)	(0.47	) (0.0	63) (0	0.79)	(0.94)	(1.06)	(1.18)	
			mm <sup>2</sup>	36.6	58.0	84.3	15	57	245	353	459	561	
Rod en	fective cross-sectional area	A <sub>se</sub>	(in. <sup>2</sup> )	(0.057)	(0.090)	(0.13	(0.2	(0	.380)	(0.547)	(0.711)	(0.870)	
		N <sub>sa</sub>	kN	18.3	29.0	42.0	78	3.5 1	22.5	176.5	229.5	280.5	
	Nominal strength as governed		(lb)	(4,114)	(6,519)	(9,476	6) (17,0	647) (27	7,539)	(39,679)	(51,594)	(63,059)	
_	by steel strength	17	kN	11.0	14.5	25.5	47	.0	73.5	106.0	137.5	168.5	
98-1 5.8		V <sub>sa</sub>	(lb)	(2,648)	(3,260)	(5,68	5) (10,	588) (16	6,523)	(23,807)	(30,956)	(37,835)	
SO 898-1 Class 5.8	Reduction for seismic shear	$lpha_{V,seis}$				•		1.00	•				
<u> </u>	Strength reduction factor for tension <sup>2</sup>	φ	-					0.65					
	Strength reduction factor for shear <sup>2</sup>	φ						0.60					
			kN	29.3	46.5	67.5	12	5.5 1	96.0	282.5	367.0	449.0	
	Nominal strength as governed	N <sub>sa</sub>	(lb)	(6,582)	(10,431)	(15,16	1) (28,	236) (44	4,063)	(63,486)	(82,550)	(100,894)	
	by steel strength		kN	17.6	23.0	40.5	75	5.5 1	17.5	169.5	220.5	269.5	
98-1		V <sub>sa</sub>	(lb)	(3,949)	(5,216)	(9,09	7) (16,	942) (26	6,438)	(38,092)	(49,530)	(60,537)	
SO 898-1 Class 8.8	Reduction for seismic shear	αv,seis	-		· ·	1.00							
<u>n</u> 0	Strength reduction factor for tension <sup>2</sup>	φ	1				0.65						
	Strength reduction factor for shear <sup>2</sup>	φ	-										
			kN	25.6	40.6	59.0	109	9.9 1	71.5	247.1	229.5	280.5	
	Nominal strength as governed	N <sub>sa</sub>	(lb)	(5,760)	(9,127)	(13,26	6) (24,	706) (38	3,555)	(55,550)	(51,594)	(63,059)	
ass 3	by steel strength		kN	15.4	20.3	35.4	65	i.9 1	02.9	148.3	137.7	168.3	
1 Cla		$V_{sa}$	(lb)	(3,456)	(4,564)	(7,960	) (14,	824) (23	3,133)	(33,330)	(30,956)	(37,835)	
SO 3506-1 Class A4 Stainless <sup>3</sup>	Reduction for seismic shear	αv,seis	-				·	0.80	I	<u> </u>	1		
ISO A	Strength reduction factor for tension <sup>2</sup>	φ	-					0.65					
	Strength reduction factor for shear <sup>2</sup>	φ	-					0.60					
DESIG	N INFORMATION	Symbol	Units			N	ominal rein	forcing bar	diameter (	mm)			
DEGIG	IT III ONIMATION	Symbol	Units	10	12	14	16	20	25	28	30	32	
Nomina	al bar diameter	d	mm	10.0	12.0	14.0	16.0	20.0	25.0	28.0	30.0	32.0	
			(in.)	(0.394)	(0.472)	(0.551)	(0.630)	(0.787)	(0.984)	(1.102)		(1.260)	
Bar effe	ective cross-sectional area	Ase	mm <sup>2</sup>	78.5	113.1	153.9	201.1	314.2	490.9	615.8	706.9	804.2	
	T		(in.²)	(0.122)	(0.175)	(0.239)	(0.312)	(0.487)	(0.761)	(0.954)	` ′	(1.247)	
		N <sub>sa</sub>	kN	43.0	62.0	84.5	110.5	173.0	270.0	338.5	388.8	442.5	
000	Nominal strength as governed		(lb)	(9,711)	(13,984)	(19,034)	(24,860)	(38,844)	(60,694)		, , , ,	(99,441)	
50/5	by steel strength	V <sub>sa</sub>	kN	26.0	37.5	51.0	66.5	103.0	162.0	203.0	233.3	265.5	
St 5		Su	(lb)	(5,827)	(8,390)	(11,420)	(14,916)	(23,307)	(36,416)	(45,681	) (52,444)	(59,665)	
38 B	Reduction for seismic shear		-					0.70					
DIN 488 BSt 550/500	Strength reduction factor for tension <sup>2</sup>	φ	-					0.65					
_	Strength reduction factor for shear <sup>2</sup>	φ	-					0.60					

¹ Values provided for common rod and rebar material types are based on specified strengths and calculated in accordance with ACI 318-19 Eq. (17.6.1.2) and Eq. (17.7.1.2b), ACI 318-14 Eq (17.4.1.2) or Eq (17.5.1.2b) or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must be appropriate for the rod.
² For use with the load combinations of Section 1605.1 of the 2021 IBC or Section 1605.2 of the 2018, 2015, and 2012 IBC, ACI 318 (-19 or -14) 5.3, or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of 
∅ must be determined in accordance with ACI 318-11 D.4.4. Values correspond to a brittle steel element.
³ A4-70 Stainless (M8- M24); A4-502 Stainless (M27- M30)







Metric Threaded Rod and EU Metric Reinforcing Bars

**Concrete Breakout Strength** 

Carbide Bit or Hilti Hollow Carbide Bit Diamond Core Bit + Roughening Tool, or Diamond Core Bit

## TABLE 15—CONCRETE BREAKOUT DESIGN INFORMATION FOR METRIC THREADED ROD AND EU METRIC REINFORCING BARS ALL DRILLING METHODS<sup>1</sup>

						Nominal r	od diame	ter (mm)			
DESIGN INFORMATION	Symbol	Units	8	10	12	16	20		24	27	30
Minimum Embedment	h	mm	60	60	70	80	90	) 1	100	110	120
	h <sub>ef,min</sub>	(in.)	(2.4)	(2.4)	(2.8)	(3.1)	(3.5	5) (3	3.9)	(4.3)	(4.7)
Maximum Embedment	h <sub>ef,max</sub>	mm	160	200	240	320	40	0 4	180	540	600
	r et,max	(in.)	(6.3)	(7.9)	(9.4)	(12.6)	(15.	7) (1	8.9)	(21.4)	(23.7)
Min. anchor spacing <sup>3</sup>	S <sub>min</sub>	mm	40	50	60	80	10	0 1	120	135	150
		(in.)	(1.6)	(2.0)	(2.4)	(3.2)	(3.9	9) (4	4.7)	(5.3)	(5.9)
Min. edge distance <sup>3</sup>	Cmin	-	5d; or s	ee Section	4.1.9 of th	is report fo	or design v	vith reduce	ed minim	ım edge di	stances
Minimum concrete thickness	6	mm	h <sub>ef</sub> +	30				h <sub>ef</sub> + 2d <sub>o</sub> (4	)		
Minimum concrete thickness	h <sub>min</sub>	(in.)	(h <sub>ef</sub> +	1 <sup>1</sup> / <sub>4</sub> )				Tlef + ZUo'	,		
DESIGN INFORMATION	Symbol	Units			Nomi	nal reinfor	cing bar	diameter (	(mm)		
DESIGN INFORMATION	Symbol	Units	10	12	14	16	20	25	28	30	32
Minimum Embedment	h <sub>ef,min</sub>	mm	60	70	80	80	90	100	112	120	128
	l let,min	(in.)	(2.4)	(2.8)	(3.1)	(3.1)	(3.5)	(3.9)	(4.4)	(4.7)	(5.0)
Maximum Embedment	h <sub>ef,max</sub>	mm	200	240	280	320	400	500	560	600	640
	· · ei,iiiax	(in.)	(7.9)	(9.4)	(9.4) (11.0) (12.6) (15.7) (19.7) (22.0) (23.7)				(25.2)		
Min. anchor spacing <sup>3</sup>	S <sub>min</sub>	mm	50	60	70	80	100	125	140	150	160
		(in.)	(2.0)	(2.4)	(2.8)	(3.2)	(3.9)	(4.9)	(5.5)	(5.9)	(6.3)
Min. edge distance <sup>3</sup>	Cmin	-	5d; or s	ee Section	4.1.9 of th	is report fo	or design v	vith reduce	ed minim	um edge di	stances
Minimum concrete thickness	h.	mm	h <sub>ef</sub> + 30				h	+ 2d <sub>o</sub> (4)			
	h <sub>min</sub>	(in.)	$(h_{ef} + 1^1/_4)$	)			Hef	- ZU <sub>0</sub> . /			
Critical edge distance – splitting (for uncracked concrete)	Cac	-			S	ee Section	4.1.10 of	this report	<b>.</b> .		
Effectiveness factor for	,	SI					7.1				
cracked concrete	Kana										
Effectiveness factor for		SI					10				
uncracked concrete	K <sub>c,uncr</sub>	(in-lb)					(24)				
Strength reduction factor for tension, concrete failure modes <sup>2</sup>	φ	-					0.65				
Strength reduction factor for shear, concrete failure modes <sup>2</sup>	φ	-					0.70				

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

<sup>1</sup>Additional setting information is described in Figure 8A and 8B, Manufacturers Printed Installation Instructions (MPII).

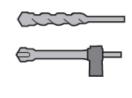
<sup>&</sup>lt;sup>2</sup> The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, the appropriate strength reduction factor must be determined in accordance with ACI 318-11 D.4.4.

³For installations with 1³/₄-inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

<sup>&</sup>lt;sup>4</sup>  $d_0$  = hole diameter.







**EU Metric Reinforcing Bars** 

**Bond Strength** 

Carbide Bit or Hilti Hollow Carbide Bit

TABLE 16—BOND STRENGTH DESIGN INFORMATION FOR EU METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT)1

		N HOLES DRILLED WIT								diameter (			
DESIG	INFORMAT	ON	Symbol	Units	10	12	14	16	20	25	28	30	32
			,	mm	60	70	80	80	90	100	112	120	128
Minimi	um Embedmen	I	h <sub>ef,min</sub>	(in.)	(2.4)	(2.8)	(3.1)	(3.1)	(3.5)	(3.9)	(4.4)	(4.7)	(5.0)
Massina	Cash a das sa		-	mm	200	240	280	320	400	500	560	600	640
waxim	um Embedmer		h <sub>ef,max</sub>	(in.)	(7.9)	(9.4)	(11.0)	(12.6)	(15.7)	(19.7)	(22.0)	(23.7)	(25.2)
		Characteristic bond strength		MPa	9.3	9.4	9.5	9.6	9.7	9.8	9.7	9.5	9.3
0	Temperature	in cracked concrete	Tk,cr	(psi)	(1,350)	(1,360)	(1,380)	(1,390)	(1,410)	(1,420)	(1,400)	(1,370)	(1,350)
y crete	range A <sup>2</sup>	Characteristic bond strength		MPa	12.2	12.1	12.0	11.8	11.6	11.4	11.2	11.1	11.0
and		in uncracked concrete	Tk,uncr	(psi)	(1,770)	(1,750)	(1,730)	(1,720)	(1,690)	(1,650)	(1,620)	(1,610)	(1,590)
crete		Characteristic bond strength		MPa	6.4	6.5	6.5	6.6	6.7	6.8	6.7	6.5	6.4
Dry concrete and Water saturated concrete	Temperature	in cracked concrete	$\tau_{k,cr}$	(psi)	(930)	(940)	(950)	(960)	(970)	(980)	(970)	(950)	(930)
Dry er s	range B <sup>2</sup>	Characteristic bond strength		MPa	8.4	8.3	8.3	8.2	8.0	7.8	7.7	7.7	7.6
Wat		in uncracked concrete	Tk,uncr	(psi)	(1,220)	(1,210)	(1,200)	(1,190)	(1,160)	(1,140)	(1,120)	(1,110)	(1,100)
	Anchor Catego	ory	-		1	1	1	1	1	1	1	1	1
	Strength Reduction factor		φ <sub>d</sub> , φ <sub>ws</sub>		0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	Strength Reduction factor  Characteristic bond streng in cracked concrete			MPa	6.9	6.9	7.0	7.2	7.4	7.4	7.4	7.4	7.2
	Temperature range A <sup>2</sup>		Tk,cr	(psi)	(1,000)	(1,010)	(1,020)	(1,040)	(1,070)	(1,080)	(1,080)	(1,070)	(1,050)
		Characteristic bond strength in uncracked concrete		MPa	9.0	8.9	8.9	8.9	8.8	8.7	8.6	8.6	8.6
<u>e</u>			T <sub>k,uncr</sub>	(psi)	(1,310)	(1,300)	(1,280)	(1,280)	(1,270)	(1,250)	(1,250)	(1,250)	(1,240)
Water-filled hole		Characteristic bond strength		MPa	4.7	4.8	4.8	5.0	5.1	5.1	5.1	5.1	5.0
ter-fille	Temperature	in cracked concrete	$ au_{k,cr}$	(psi)	(690)	(700)	(700)	(720)	(740)	(740)	(740)	(740)	(720)
Wa	range B <sup>2</sup>	Characteristic bond strength		MPa	6.2	6.2	6.1	6.1	6.1	6.0	5.9	5.9	5.9
		in uncracked concrete	Tk,uncr	(psi)	(900)	(890)	(890)	(890)	(880)	(870)	(860)	(860)	(860)
	Anchor Catego	ory	-	-	3	3	3	3	3	3	3	3	3
	Strength Redu	ction factor	фwf	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
		Characteristic bond strength		MPa	6.0	6.1	6.2	6.3	6.6	6.8	6.8	6.8	6.8
	Temperature	in cracked concrete	Tk,cr	(psi)	(880)	(890)	(890)	(920)	(960)	(980)	(980)	(990)	(980)
rete	range A <sup>2</sup>	Characteristic bond strength	Tk,uncr	MPa	7.9	7.8	7.8	7.8	7.9	7.8	7.9	8.0	8.0
onc		in uncracked concrete	ck,unci	(psi)	(1,140)	(1,140)	(1,130)	(1,140)	(1,140)	(1,140)	(1,140)	(1,150)	(1,160)
ed c		Characteristic bond strength in cracked concrete	Tk,cr	MPa	4.2	4.2	4.3	4.4	4.6	4.7	4.7	4.7	4.7
nerg	Temperature range B <sup>2</sup>			(psi) MPa	(600) 5.4	(610) 5.4	(620) 5.4	(630) 5.4	(660) 5.4	(680) 5.4	(680) 5.4	(680) 5.5	(680) 5.5
Submerged concrete	range b	Characteristic bond strength in uncracked concrete	Tk,uncr	(psi)	(790)	(780)	(780)	(790)	(790)	(780)	(790)	(800)	(800)
0,	Anabar Cata			\ ' '	` ′	,	` '	` ′	` '	, ,	` '	,	` ,
	Anchor Catego	•	-	-	3	3	3	3	3	3	3	3	3
Doduc	Strength Redu		φuw	-	0.45	0.45 0.9	0.45 0.9	0.45	0.45 0.9	0.45 0.9	0.45 0.9	0.45 0.9	0.45
Reduc	uon ioi seismic	IEHSIUH	CLN, seis	-	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9	0.9

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c/17.2)^{0.15}$ ]. See Section 4.1.4 of this report for bond strength determination.

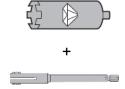
<sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







**EU Metric Reinforcing Bars** 

**Bond Strength** 

Diamond Core Bit + **Roughening Tool** 

#### TABLE 17—BOND STRENGTH DESIGN INFORMATION FOR EU METRIC REINFORCING BARS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL1

DEGLO	NUNCORMAT	ION	0	11		Nominal rei	nforcing bar dia	ameter (mm)	
DESIG	N INFORMAT	ION	Symbol	Units	14	16	20	25	28
Minimu	m Embedmen	•	h	mm	80	80	90	100	112
wimimu	m Embeamen	L	h <sub>ef,min</sub>	(in.)	(3.1)	(3.1)	(3.5)	(3.9)	(4.4)
Mavim	ım Embedmer	.+	h	mm	280	320	400	500	560
Maximi	ını Embedinei		h <sub>ef,max</sub>	(in.)	(11.0)	(12.6)	(15.7)	(19.7)	(22.0)
		Characteristic bond		MPa	6.7	6.7	6.8	6.9	6.8
ete	strength in cracked concrete range A <sup>2</sup> Characteristic bond strength in uncracket		$ au_{k,cr}$	(psi)	(965)	(970)	(985)	(995)	(980)
oncr	range A <sup>2</sup>		_	MPa	12.0	11.8	11.6	11.4	11.2
		concrete	Tk,uncr	(psi)	(1,730)	(1,720)	(1,690)	(1,650)	(1,620)
saturated		Characteristic bond		MPa	4.6	4.6	4.7	4.8	4.7
	Temperature	strength in cracked concrete	Tk,cr	(psi)	(665)	(670)	(680)	(685)	(680)
d water	range B <sup>2</sup>	Characteristic bond		MPa	8.3	8.2	8.0	7.8	7.7
y and		strength in uncracked concrete	Tk,uncr	(psi)	(1,200)	(1,190)	(1,160)	(1,140)	(1,120)
Dry	Anchor Categ	jory	-	-	1	1	1	1	1
	Strength Reduction factor		φd, φws	-	0.65	0.65	0.65	0.65	0.65
Reduct	ion for seismic	αN,seis	-	0.9	0.9	0.9	0.9	0.9	

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa. For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength in the range 2,500 psi ≤ f'c ≤ 8,000 psi). <sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C). Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







**EU Metric Reinforcing Bars** 

**Bond Strength** 

**Diamond Core Bit** 

#### TABLE 18—BOND STRENGTH DESIGN INFORMATION FOR EU METRIC REINFORCING BARS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT1

							Non	ninal reinfo	orcing bar	diameter (	(mm)		
DESIGN	INFORMATION		Symbol	Units	10	12	14	16	20	25	28	30	32
Minimum	Embodment		<b>b</b>	mm	60	70	80	80	90	100	112	120	128
WIIIIIIIIIIII	Embedment		h <sub>ef,min</sub>	(in.)	(2.4)	(2.8)	(3.1)	(3.1)	(3.5)	(3.9)	(4.4)	(4.7)	(5.0)
Mavimun	aximum Embedment		h -	mm	200	240	280	320	400	500	560	600	640
waxiiiiuii	Maximum Embedment		h <sub>ef,max</sub>	(in.)	(7.9)	(9.4)	(11.0)	(12.6)	(15.7)	(19.7)	(22.0)	(23.7)	(25.2)
Ţ,	Temperature Characteristic bond strength in uncracked		Tk.uncr	MPa	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0	8.0
turate	range A <sup>2</sup>	concrete	Tk,uncr	(psi)	(1,150)	(1,150)	(1,150)	(1,150)	(1,150)	(1,150)	(1,150)	(1,150)	(1,150)
ter Sa crete	Temperature range A <sup>2</sup> strength in uncracked concrete  Temperature range B <sup>2</sup> Characteristic bond strength in uncracked concrete			MPa	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5
d Wat	Temperature range B <sup>2</sup> strength in uncracked concrete  Anchor Category		Tk,uncr	(psi)	(800)	(800)	(800)	(800)	(800)	(800)	(800)	(800)	(800)
ry an	Anchor Category		-		2	2	2	3	3	3	3	3	3
	Strength Reduction factor		$\phi_{\sf d}$ , $\phi_{\sf ws}$		0.55	0.55	0.55	0.45	0.45	0.45	0.45	0.45	0.45

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

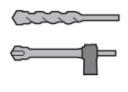
Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c/17.2)^{0.25}$ ]. See Section 4.1.4 of this report for bond strength determination.

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C). Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).







**Metric Threaded Rod** 

**Bond Strength** 

Carbide Bit or Hilti Hollow Carbide Bit

TABLE 19—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED RODS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT)

Page 19   Page 19   Page 29   Page						, -			lominal rod		n)		
Maximum Embedment   Maxi	DESI	GN INF	FORMATION	Symbol	Units	8	10	12	16	20	24	27	30
Maximum Embedment	Minin	num Em	nhedment	h.	mm	60	60	70	80	90	100	110	120
Page 19   Page	IVIIIIIII	IUIII LII	ibedifient	I lef,min	(in.)	` ′	` ,	. ,	. ,	, ,	. ,	` '	_ ` _
Characteristic bond strength in cracked concrete   R_ccr   (psi)   (1,280)   (1,280)   (1,270)   (1,260)   (1,250)   (1,240)   (1,230)   (1,220)	Maxir	mum Er	mbedment	h <sub>ef max</sub>									
Page			_	11CI,IIIdX					` ,	, ,			, ,
Part	Φ	<u>e</u>		Ti. au	MPa	8.8	8.8	8.8	8.7	8.6	8.5	8.5	8.4
Part	cret	e A		ık,cr	(psi)	(1,280)	(1,280)	(1,270)	(1,260)	(1,250)	(1,240)	(1,230)	(1,220)
Part	Con	mpe			MPa	16.7	16.3	16.0	15.2	14.5	13.8	13.2	12.7
Strength Reduction factor	ted	Te T		Tk,uncr	(psi)	(2,420)	(2,370)	(2,320)	(2,210)	(2,100)	(2,000)	(1,920)	(1,840)
Strength Reduction factor	tura	Φ			MPa	6.1	6.1	6.0	6.0	5.9	5.9	5.9	5.8
Strength Reduction factor	Š	ratur B <sup>2</sup>		Tk,cr	(psi)	(890)	(880)	(880)	(870)	(860)	(860)	(850)	(840)
Strength Reduction factor	Nate	npel			MPa	11.5	11.3	11.0	10.5	10.0	9.5	9.1	8.7
Strength Reduction factor	nd /	Ter		$ au_{k,uncr}$	(psi)	(1,670)	(1,630)	(1,600)	(1,520)	(1,450)	(1,380)	(1,320)	(1,270)
Strength Reduction factor	Jry 8			-	_	1	1	1	1	1	1	1	1
Part			<u> </u>	Ød. Øws	-			0.65					0.65
Characteristic bond strength in cracked concrete   Characteristic bond strength in uncracked concrete   Characteristic bond strength in cracked concrete   Characteristic bond strength in uncracked   Characteristic bond strength in uncracked   Characteristic bond strength in uncracked   Characteristic bond   Characteristi		n o	Characteristic bond	7 - 7 -	MPa	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.5
Characteristic bond strength in cracked concrete   Characteristic bond strength in uncracked concrete   Characteristic bond strength in cracked concrete   Characteristic bond strength in uncracked   Characteristic bond strength in uncracked   Characteristic bond strength in uncracked   Characteristic bond   Characteristi		ature A <sup>2</sup>		Tk,cr	(psi)	(940)	(940)	(940)	(940)	(940)	(940)	(950)	(950)
Characteristic bond strength in cracked concrete   Characteristic bond strength in uncracked concrete   Characteristic bond strength in cracked concrete   Characteristic bond strength in uncracked   Characteristic bond strength in uncracked   Characteristic bond strength in uncracked   Characteristic bond   Characteristi		nper	Characteristic bond		MPa	12.3	12.1	11.8	11.4	11.0	10.5	10.2	9.8
Strength in uncracked concrete   Tik,uncr   (psi)   (1,230)   (1,210)   (1,180)   (1,140)   (1,140)   (1,100)   (1,050)   (1,020)   (990)	ole	Ter		Tk,uncr	(psi)	(1,780)	(1,750)	(1,710)	(1,650)	(1,590)	(1,520)	(1,470)	(1,430)
Strength in uncracked concrete   Tik,uncr   (psi)   (1,230)   (1,210)   (1,180)   (1,140)   (1,140)   (1,100)   (1,050)   (1,020)   (990)	ed	d)			MPa	4.5	4.5	4.5	4.5	4.5	4.5	4.5	4.5
Strength in uncracked concrete   Tik,uncr   (psi)   (1,230)   (1,210)   (1,180)   (1,140)   (1,140)   (1,100)   (1,050)   (1,020)   (990)	er-fil	atur B <sup>2</sup>		Tk,cr	(psi)	(650)	(650)	(650)	(650)	(650)	(650)	(650)	(650)
Anchor Category  Anchor	Wat	npel	Characteristic bond		MPa	8.5	8.3	8.2	7.9	7.6	7.2	7.0	6.8
Anchor Category  Strength Reduction factor  Strength Reduction factor  Strength Reduction factor  Anchor Category  3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		Ter		$ au_{k,uncr}$	(psi)	(1,230)	(1,210)	(1,180)	(1,140)	(1,100)	(1,050)	(1,020)	(990)
Characteristic bond strength in cracked concrete  Characteristic bond strength in uncracked concrete  Characteristic bond strength in characteristic bond strength in characteristic bond strength in characteristic bond strength in cracked concrete  Characteristic bond strength in characteristic bond strength in cracked concrete  Characteristic bond strength in uncracked concrete  Characteristic bond strength in cracked concrete  Ch		Anchor	l .	-	-	3	3	3	3	3	3	3	3
Strength in cracked concrete		Streng	th Reduction factor	фwf	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Characteristic bond strength in cracked concrete  MPa 3.9 3.9 3.9 4.0 4.0 4.1 4.1 4.1 4.2   (psi) (570) (570) (570) (580) (580) (590) (600		Φ			MPa	5.7	5.7	5.7	5.7	5.8	5.9	6.0	6.0
Characteristic bond strength in cracked concrete  MPa 3.9 3.9 3.9 4.0 4.0 4.1 4.1 4.1 4.2   (psi) (570) (570) (570) (580) (580) (590) (600		atur A²		Tk,cr	(psi)	(820)	(820)	(830)	(830)	(840)	(860)	(870)	(870)
Characteristic bond strength in cracked concrete  MPa 3.9 3.9 3.9 4.0 4.0 4.1 4.1 4.1 4.2   (psi) (570) (570) (570) (580) (580) (590) (600	, e	nper ange	Characteristic bond		MPa	10.7	10.5	10.4	10.1	9.8	9.5	9.3	9.1
Concrete   (psi) (1,070) (1,060) (1,040) (1,010) (980) (950) (930) (910)	ncref	Ter T		Tk,uncr	(psi)	(1,550)	(1,530)	(1,500)	(1,460)	(1,420)	(1,380)	(1,350)	(1,320)
Concrete   (psi) (1,070) (1,060) (1,040) (1,010) (980) (950) (930) (910)	<u>0</u>	Φ.	Characteristic bond		MPa	3.9	3.9	3.9	4.0	4.0	4.1	4.1	4.2
Concrete   (psi) (1,070) (1,060) (1,040) (1,010) (980) (950) (930) (910)	erge	ratur B <sup>2</sup>		Tk,cr	(psi)	(570)	(570)	(570)	(580)	(580)	(590)	(600)	(600)
Concrete   (psi) (1,070) (1,060) (1,040) (1,010) (980) (950) (930) (910)	pmqr	npel	Characteristic bond		MPa	7.4	7.3	7.2	7.0	6.8	6.6	6.4	6.3
Strength Reduction factor φ <sub>uw</sub> - 0.45 0.45 0.45 0.45 0.45 0.45 0.45	ઌ	Ter T		Tk,uncr	(psi)	(1,070)	(1,060)	(1,040)	(1,010)	(980)	(950)	(930)	(910)
700		Ancho	Category	-	-	3	3	3	3	3	3	3	3
Reduction for seismic tension $\alpha_{N,seis}$ - 1 0.92 0.93 0.95 1 1 1		Streng	th Reduction factor	$\phi_{uw}$	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
	Redu	ction fo	r seismic tension	αN,seis	-	1	0.92	0.93	0.95	1	1	1	1

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c/17.2)^{0.15}$ ]. See Section 4.1.4 of this report for bond strength determination.

<sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant pariety extracted of time.

constant over significant periods of time.







**Metric Threaded Rod** 

**Bond Strength** 

Diamond Core Bit + Roughening Tool

#### TABLE 20—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED RODS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL<sup>1</sup>

DEC	ION INFORMA	TION	Oh al	l luita		Nomi	nal rod diameter	(mm)	
DES	IGN INFORMA	TION	Symbol	Units	16	20	24	27	30
Minin	num Embedme	.mt	6	mm	80	90	100	110	120
IVIIIIII	num Embeame	erit	h <sub>ef,min</sub>	(in.)	(3.1)	(3.5)	(3.9)	(4.3)	(4.7)
Movi	mum Embedme	ant	h	mm	320	400	480	540	600
IVIAXI	mum Embeum	ent	h <sub>ef,max</sub>	(in.)	(12.6)	(15.7)	(18.9)	(21.4)	(23.7)
ete		Characteristic bond trength		MPa	6.1	6.0	6.0	6.0	5.9
concrete	Temp.	in cracked concrete	Tk,cr	(psi)	(880)	(875)	(870)	(860)	(855)
	range A <sup>2</sup>	Characteristic bond trength	_	Мра	15.2	14.5	13.8	13.2	12.7
ated		in uncracked concrete	Tk,uncr	(psi)	(2,210)	(2,100)	(2,000)	(1,920)	(1,840)
saturated		Characteristic bond trength	_	MPa	4.2	4.2	4.2	4.2	4.1
	Temp.	in cracked concrete	Tk,cr	(psi)	(610)	(605)	(600)	(595)	(590)
ate	range B <sup>2</sup>	Characteristic bond trength	_	MPa	10.5	10.0	9.5	9.1	8.7
and water	in uncracked concrete		Tk,uncr	(psi)	(1,520)	(1,450)	(1,385)	(1,320)	(1,270)
/an	Anchor Category		-	-	1	1	1	1	1
Dry	Strength Re	duction factor	φ <sub>d</sub> , φ <sub>ws</sub>	-	0.65	0.65	0.65	0.65	0.65
Redu	ction for seism	ic tension	$lpha_{N, { m seis}}$	-	0.95	1	1	1	1

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







Metric Threaded Rod

**Bond Strength** 

**Diamond Core Bit** 

#### TABLE 21—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED RODS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT1

DECION	INICODMATI	ON.	0	Unita			No	minal rod o	liameter (n	nm)		
DESIGN	INFORMATION	UN	Symbol	Units	8	10	12	16	20	24	27	30
Minimum	Embedment		h.	mm	60	60	70	80	90	100	110	120
wiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiiii	Lilibedillelit		h <sub>ef,min</sub>	(in.)	(2.4)	(2.4)	(2.8)	(3.1)	(3.5)	(3.9)	(4.3)	(4.7)
Massimassin	aximum Embedment		h <sub>ef.max</sub>	mm	160	200	240	320	400	480	540	600
Maximum	Maximum Embedment			(in.)	(6.3)	(7.9)	(9.4)	(12.6)	(15.7)	(18.9)	(21.4)	(23.7)
	Temp. Characteristic bond strength		_	MPa	10.7	10.7	10.7	10.7	10.7	10.7	10.7	10.7
a te	range A <sup>2</sup>	in uncracked concrete	Tk,uncr	(psi)	(1,550)	(1,550)	(1,550)	(1,550)	(1,550)	(1,550)	(1,550)	(1,550)
and atur rete	put ange A² in uncracked concrete  Temp. Characteristic bond strength in uncracked concrete  Temp. In uncracked concrete in uncracked concrete			MPa	7.4	7.4	7.4	7.4	7.4	7.4	7.4	7.4
> o ≥	> 0 El range R <sup>2</sup> lin uncracked concrete		Tk, uncr	(psi)	(1,070)	(1,070)	(1,070)	(1,070)	(1,070)	(1,070)	(1,070)	(1,070)
L Vate	Anchor Category		-	-	2	2	2	3	3	3	3	3
>	Strength Reduction factor		φ <sub>d</sub> , φ <sub>ws</sub>	-	0.55	0.55	0.55	0.45	0.45	0.45	0.45	0.45

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of (f<sub>c</sub> / 2,500)<sup>0.25</sup> for uncracked concrete [For SI: (f<sub>c</sub> / 17.2)<sup>0.25</sup>]. See Section 4.1.4 of this report for bond strength determination.

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

 $<sup>^{1}</sup>$ Bond strength values correspond to concrete compressive strength in the range 2,500 psi  $\leq$  f'c  $\leq$  8,000 psi).

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C). Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).



Canadian Reinforcing Bars

Steel Strength

#### TABLE 22—STEEL DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS1

DEC	IGN INFORMATION	Cumbal	Units		Nomin	al reinforcing b	ar size		
DES	IGN INFORMATION	Symbol	Units	10 M	15 M	20 M	25 M	30 M	
Nom	inal bar diameter	d	mm	11.3	16.0	19.5	25.2	29.9	
NOIII		u	(in.)	(0.445)	(0.630)	(0.768)	(0.992)	(1.177)	
Por	effective cross-sectional area	Ase	mm²	100.3	201.1	298.6	498.8	702.2	
Dai	enective cross-sectional area	Ase	(in.²)	(0.155)	(0.312)	(0.463)	(0.773)	(1.088)	
		Nsa	kN	54.0	108.5	161.5	270.0	380.0	
	Nominal strength as governed by steel	IVsa	(lb)	(12,175)	(24,408)	(36,255)	(60,548)	(85,239)	
0	strength	Vsa	kN	32.5	65.0	97.0	161.5	227.5	
G30		V sa	(lb)	(7,305)	(14,645)	(21,753)	(36,329)	(51,144)	
CSA	Reduction for seismic shear	αv,seis	-			0.70			
O	Strength reduction factor for tension <sup>2</sup>	φ	-	0.65					
Strength reduction factor for shear <sup>2</sup>		φ	-	0.60					

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

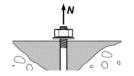
For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

1 Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. (17.6.1.2) and Eq. (17.7.1.2b), ACI

318-14 Eq (17.4.1.2) or Eq (17.5.1.2b) or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Other material specifications are admissible.

2For use with the load combinations of ACI 318 (-19 or -14) 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable.







Canadian Reinforcing Bars

Concrete Breakout Strength

Carbide Bit or Hilti Hollow Carbide Bit or Diamond Core Bit

#### TABLE 23—CONCRETE BREAKOUT DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT), OR DIAMOND CORE BIT1

DESIGN INFORMATION	Cumhal	Unita		Nonm	inal reinforcing b	ar size		
DESIGN INFORMATION	Symbol	Units	10 M	15 M	20 M	25 M	30 M	
Effectiveness factor for cracked concrete	le.	SI			7.1			
Ellectiveness factor for cracked concrete	k <sub>c,cr</sub>	(in-lb)			(17)			
Effectiveness factor for uncracked concrete	k	SI			10			
	K <sub>c,uncr</sub>	(in-lb)			(24)			
Minimum Embedment	h.	mm	60	80	90	101	120	
	h <sub>ef,min</sub>	(in.)	(2.4)	(3.1)	(3.5)	(4.0)	(4.7)	
Maximum Embedment	h .	mm	226	320	390	504	598	
Maximum Embedment	h <sub>ef,max</sub>	(in.)	(8.9)	(12.6)	(15.4)	(19.8)	(23.5)	
Min har angaing?		mm	57	80	98	126	150	
Min. bar spacing <sup>3</sup>	Smin	(in.)	(2.2)	(3.1)	(3.8)	(5.0)	(5.9)	
Min. edge distance <sup>3</sup>		mm	Eduar and Conti	ion 110 of this ro	port for design with	raduaad minimum	a adaa diatanaa	
wiiri. edge distance	Cmin	(in.)	ou, or see secti	1011 4.1.9 01 11115 16	port for design with	reduced minimum	reuge distances	
Minimum concrete thickness	h .	mm	h <sub>ef</sub> + 30		h <sub>ef</sub> +	2d (4)		
Willimum Concrete unickness	h <sub>min</sub>	(in.)	$(h_{ef} + 1^{1}/_{4})$		∏ef ⊤	2 <b>u</b> <sub>0</sub> , /		
Critical edge distance – splitting (for uncracked concrete)	Cac	-		See Se	ection 4.1.10 of this	s report.		
Strength reduction factor for tension, concrete failure modes <sup>2</sup>	φ	-			0.65			
Strength reduction factor for shear, concrete failure modes <sup>2</sup>	φ	-	- 0.70					

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 8A, Manufacturers Printed Installation Instructions (MPII).

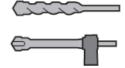
<sup>&</sup>lt;sup>2</sup> The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, the appropriate strength reduction factor must be determined in accordance with ACI 318-11 D.4.4.

<sup>&</sup>lt;sup>3</sup>For installations with 1<sup>3</sup>/<sub>4</sub>-inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements

 $<sup>^{4}</sup>$   $d_{0}$  = hole diameter.







Canadian Reinforcing Bars

**Bond Strength** 

Carbide Bit or Hilti Hollow Carbide Bit

#### TABLE 24—BOND STRENGTH DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT) 1

						•	nal reinforcing ba		
DESIGN	INFORMATION		Symbol	Units	10M	15M	20M	25M	30M
				mm	60	80	90	101	120
Minimum	Embedment		h <sub>ef,min</sub>	(in.)	(2.4)	(3.1)	(3.5)	(4.0)	(4.7)
Maximum	n Embedment		h <sub>ef,max</sub>	mm	226	320	390	504	598
	Linbedinent		I let,max	(in.)	(8.9)	(12.6)	(15.4)	(19.8)	(23.5)
crete		Characteristic bond strength in cracked	Tk,cr	MPa	9.4	9.6	9.7	9.8	9.5
Sonc	Temperature	concrete	tk,cr	(psi)	(1,360)	(1,390)	(1,410)	(1,420)	(1,380)
ted (	range A <sup>2</sup>	Characteristic bond		MPa	12.1	11.8	11.7	11.3	11.1
concrete and Water Saturated Concrete		strength in uncracked concrete	$ au_{k,uncr}$	(psi)	(1,760)	(1,720)	(1,690)	(1,650)	(1,610)
er S		Characteristic bond strength in cracked	Tk,cr	MPa	6.5	6.6	6.7	6.8	6.5
Wat	Temperature	concrete	tk,cr	(psi)	(940)	(960)	(970)	(980)	(950)
and	range B²	Characteristic bond		MPa	8.4	8.2	8.0	7.8	7.7
rete		strength in uncracked concrete	Tk,uncr	(psi)	(1,210)	(1,190)	(1,170)	(1,140)	(1,110)
conc	Anchor Category		-	-	1	1	1	1	1
Dry	Strength Reducti	on factor	φ <sub>d</sub> , φ <sub>ws</sub>	-	0.65	0.65	0.65	0.65	0.65
		Characteristic bond		MPa	6.9	7.2	7.3	7.4	7.3
	Temperature	strength in cracked concrete	$\tau_{k,cr}$	(psi)	(1,010)	(1,040)	(1,060)	(1,080)	(1,060)
	range A <sup>2</sup>	Characteristic bond		MPa	8.9	8.9	8.8	8.6	8.5
<u>ole</u>		strength in uncracked concrete	Tk,uncr	(psi)	(1,300)	(1,280)	(1,270)	(1,250)	(1,240)
ed h		Characteristic bond		MPa	4.8	5.0	5.0	5.1	5.0
Water-filled hole	Temperature	strength in cracked concrete	$ au_{k,cr}$	(psi)	(700)	(720)	(730)	(740)	(730)
Wat	range B²	Characteristic bond		MPa	6.2	6.1	6.1	6.0	5.9
		strength in uncracked concrete	$\tau_{k,uncr}$	(psi)	(900)	(890)	(880)	(860)	(850)
	Anchor Category		-	-	3	3	3	3	3
	Strength Reducti	on factor	$\phi_{wf}$	-	0.45	0.45	0.45	0.45	0.45
		Characteristic bond		MPa	6.1	6.3	6.5	6.8	6.6
	Temperature	strength in cracked concrete	Tk,cr	(psi)	(880)	(920)	(940)	(980)	(960)
ø.	range A²	Characteristic bond		MPa	7.8	7.8	7.8	7.8	7.8
crete		strength in uncracked concrete	Tk,uncr	(psi)	(1,130)	(1,140)	(1,140)	(1,140)	(1,130)
Con		Characteristic bond		MPa	4.2	4.4	4.5	4.7	4.6
ergec	Temperature	strength in cracked concrete	Tk,cr	(psi)	(610)	(630)	(650)	(680)	(660)
Submerged concrete	range B <sup>2</sup>	Characteristic bond strength in uncracked	_	MPa	5.4	5.4	5.4	5.4	5.4
0)		concrete	Tk,uncr	(psi)	(780)	(790)	(780)	(780)	(780)
	Anchor Category		-	-	3	3	3	3	3
	Strength Reducti	on factor	$\phi_{uw}$	-	0.45	0.45	0.45	0.45	0.45
Reduction	n for seismic tensi	on	α <sub>N,seis</sub>	-	0.9	0.9	0.9	0.9	0.9

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

<sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c/2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c/17.2)^{0.25}$ ] and  $(f_c/2,500)^{0.15}$  for cracked concrete [For SI:  $(f_c/17.2)^{0.15}$ ]. See Section 4.1.4 of this report for bond strength determination.

<sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







**Canadian Reinforcing Bars** 

**Bond Strength** 

Diamond Core Bit + Roughening Tool

#### TABLE 25A—BOND STRENGTH DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL<sup>1</sup>

DESIGN	INFORMATION		Symbol	Units	Nominal reinfo	rcing bar size
DESIGN	TINFORMATION		Symbol	Units	15M	20M
Minimun	n Embedment		h <sub>ef,min</sub>	mm	80	90
Willillillilli	i Embedment		I lef,min	(in.)	(3.1)	(3.5)
Maximuu	m Embodmont		h <sub>ef.max</sub>	mm	320	390
waxiiiiui	ximum Embedment			(in.)	(12.6)	(15.4)
		Characteristic bond strength in	$ au_{k,cr}$	MPa	6.7	6.8
Ð	T	cracked concrete	₽K,CF	(psi)	(970)	(985)
ate	Temperature range A <sup>2</sup>	Characteristic bond strength in	_	MPa	11.8	11.7
Saturated te		uncracked concrete	Tk,uncr	(psi)	(1,720)	(1,690)
		Characteristic bond strength in	_	MPa	4.6	4.7
Water	Temperature range B <sup>2</sup>	cracked concrete	Tk,cr	(psi)	(670)	(680)
	remperature range b	Characteristic bond strength in	_	MPa	8.2	8.0
and		uncracked concrete	$\tau_{k,uncr}$	(psi)	(1,190)	(1,170)
Dry a	Anchor Category		-		1	1
	Strength Reduction factor				0.65	0.65
Reduction	on for seismic tension		$lpha_{N, { m seis}}$	-	0.9	0.9

For **SI**: 1 inch ≡ 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over order intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







Canadian Reinforcing Bars

**Bond Strength** 

**Diamond Core Bit** 

#### TABLE 25B—BOND STRENGTH DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT1

DESIGNI	INFORMATION		Symbol	Units		Nomina	al reinforcing	bar size	
DESIGN	INFORMATION		Symbol	Units	10M	15M	20M	25M	30M
Minimum	Embedment		h <sub>ef.min</sub>	mm	60	80	90	101	120
William	Litibeditient		r rer, min	(in.)	(2.4)	(3.1)	(3.5)	(4.0)	(4.7)
Maximum	Embedment		h <sub>ef.max</sub>	mm	226	320	390	504	598
IVIAXIIIIUIII	Lilibedillelit		I lef,max	(in.)	(8.9)	(12.6)	(15.4)	(19.8)	(23.5)
te	Tomporatura ranga A2	Characteristic bond strength in	_	MPa	8.0	8.0	8.0	8.0	8.0
Water concrete	Temperature range A <sup>2</sup>	uncracked concrete	$ au_{k,uncr}$	(psi)	(1,150)	(1,150)	(1,150)	(1,150)	(1,150)
Wat	Temperature range B <sup>2</sup>	Characteristic bond strength in	_	MPa	5.5	5.5	5.5	5.5	5.5
/ and ated	Temperature range b	uncracked concrete	Tk,uncr	(psi)	(800)	(800)	(800)	(800)	(800)
ory a	Anchor Category		-	-	2	3	3	3	3
Sat	Strength Reduction factor	г	φ <sub>d</sub> , φ <sub>ws</sub>	-	0.55	0.45	0.45	0.45	0.45

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of (f'c / 2,500)<sup>0.25</sup> for uncracked concrete [For SI: (f'c / 17.2)<sup>0.25</sup>]. See Section 4.1.4 of this report for bond strength determination.

<sup>&</sup>lt;sup>1</sup>Bond strength values correspond to concrete compressive strength in the range 2,500 psi ≤ f'c ≤ 8,000 psi).

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.





#### Fractional and Metric HIS-N and HIS-RN **Internal Threaded Insert**

#### Steel Strength

#### TABLE 26—STEEL DESIGN INFORMATION FOR FRACTIONAL AND METRIC HIS-N AND HIS-RN THREADED INSERTS1

DESIG	ON INFORMATION	Symbol	Units	Nomina		o Screw D actional	iameter	Units	No	ominal Bo	lt/Cap Scr mm) Metri		ter
		,		3/8	1/2	<sup>5</sup> / <sub>8</sub>	3/4		8	10	12	16	20
HIS In	sert O.D.	D	in.	0.65	0.81	1.00	1.09	mm	12.5	16.5	20.5	25.4	27.6
			(mm)	(16.5)	(20.5)	(25.4)	(27.6)	(in.)	(0.49)	(0.65)	(0.81)	(1.00)	(1.09)
HIS in	sert length	1	in.	4.33 (110)	4.92 (125)	6.69 (170)	8.07 (205)	mm (in.)	90 (3.54)	110	125 (4.92)	170 (6.69)	205
D = 14 = 1	G4:		(mm) in. <sup>2</sup>	0.0775	0.1419	0.2260	0.3345	mm <sup>2</sup>	36.6	(4.33) 58	84.3	157	(8.07) 245
	ffective cross- nal area	A <sub>se</sub>	(mm <sup>2</sup> )	(50)	(92)	(146)	(216)	(in. <sup>2</sup> )	(0.057)	(0.090)	(0.131)	(0.243)	(0.380)
HIS in	sert effective cross-		in. <sup>2</sup>	0.178	0.243	0.404	0.410	mm <sup>2</sup>	51.5	108	169.1	256.1	237.6
	nal area	Ainsert	(mm²)	(115)	(157)	(260)	(265)	(in.²)	(0.080)	(0.167)	(0.262)	(0.397)	(0.368)
	Nominal steel	Λ/	lb	9,690	17,740	28,250	41,815	kN	-	-	-	-	-
B7	strength – ASTM	N <sub>sa</sub>	(kN)	(43.1)	(78.9)	(125.7)	(186.0)	(lb)	-	-	-	-	-
193	A193 B7³ bolt/cap	V <sub>sa</sub>	lb	5,815	10,645	16,950	25,090	kN	-	-	-	-	-
Σ	screw	V sa	(kN)	(25.9)	(47.3)	(75.4)	(111.6)	(lb)	-	-	-	-	-
ASTM A193	Nominal steel strength –		lb	12,645	17,250	28,680	29,145	kN	-	-	-	-	-
	HIS-N insert	N <sub>sa</sub>	(kN)	(56.3)	(76.7)	(127.6)	(129.7)	(lb)	-	-	-	-	-
	Naminal stool	A.I	lb	8,525	15,610	24,860	36,795	kN	-	-	-	-	-
SS SS	Nominal steel strength – ASTM	N <sub>sa</sub>	(kN)	(37.9)	(69.4)	(110.6)	(163.7)	(lb)	-	-	-	-	-
ASTM A193 rade B8M S	A193 Grade B8M SS bolt/cap screw	V <sub>sa</sub>	lb	5,115	9,365	14,915	22,075	kN	-	-	-	-	-
STM de E	boll/cap screw	V sa	(kN)	(22.8)	(41.7)	(66.3)	(98.2)	(lb)	-	-	-	-	-
ASTN Grade I	Nominal steel		lb	18,065	24,645	40,970	41,635	kN	-	-	-	-	-
	strength – HIS-RN insert	N <sub>sa</sub>	(kN)	(80.4)	(109.6)	(182.2)	(185.2)	(lb)	-	-	-	-	-
	Nominal steel	N <sub>sa</sub>	lb	-	-	-	-	kN	29.5	46.5	67.5	125.5	196.0
<del>-</del> ~	strength – ISO 898-1		(kN)	-	-	-	-	(lb)	(6,582)	(10,431)	(15,161)	(28,236)	(44,063)
-868	Class 8.8 bolt/cap screw	V <sub>sa</sub>	lb	-	-	-	-	kN	17.5	28.0	40.5	75.5	117.5
ISO 898-1 Class 8.8	Sciew	V sa	(kN)	-	-	-	-	(lb)	(3,949)	(6,259)	(9,097)	(16,942)	(26,438)
<u>0</u>	Nominal steel strength –	N <sub>sa</sub>	lb	-	-	-	-	kN	25.0	53.0	83.0	125.5	116.5
	HIS-N insert	IVsa	(kN)	-	-	-	-	(lb)	(5,669)	(11,894)	(18,628)	(28,210)	(26,176)
· · ·	Nominal steel	N <sub>sa</sub>	lb	-	-	-	-	kN	25.5	40.5	59.0	110.0	171.5
Slass less	strength – ISO 3506- 1 Class A4-70	IVsa	(kN)	-	-	-	-	(lb)	(5,760)	(9,127)	(13,266)	(24,706)	(38,555)
506-1 Class 0 Stainless	Stainless bolt/cap	V <sub>sa</sub>	lb	-	-	-	-	kN	15.5	24.5	35.5	66.0	103.0
	screw	V sa	(kN)	-	-	-	-	(lb)	(3,456)	(5,476)	(7,960)	(14,824)	(23,133)
30 A4-7	Nominal steel strength –		lb	-	-	-	-	kN	36.0	75.5	118.5	179.5	166.5
<u></u>	HIS-RN insert	N <sub>sa</sub>	(kN)	-	-	-	-	(lb)	(8,099)	(16,991)	(26,612)	(40,300)	(37,394)
Reduc	ction for seismic shear	αv,seis	-		0.	94		-			0.94		
Streng for ter	yth reduction factor usion <sup>2</sup>	φ	-		0.	65		-			0.65		
Streng for she	yth reduction factor ear <sup>2</sup>	φ			0.	60		-			0.60		

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

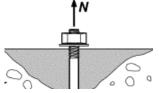
<sup>1</sup>Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-19 Eq. (17.6.1.2) and Eq. (17.7.1.2b), ACI 318-14 Eq (17.4.1.2) or Eq (17.5.1.2b) or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must be appropriate for the rod.

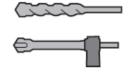
<sup>2</sup>For use with the load combinations of ACI 318 (-19 or -14) 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11

D.4.3, as applicable. Values correspond to a brittle steel element for the HIS insert.

<sup>14 17.3.3</sup> or ACI 318-11 D.4.3, as applicable, can be used







Fractional and Metric HIS-N and HIS-RN **Internal Threaded Insert** 

**Concrete Breakout Strength** 

Carbide Bit or Hilti Hollow Carbide Bit

#### TABLE 27—CONCRETE BREAKOUT DESIGN INFORMATION FOR FRACTIONAL AND METRIC HILTI HIS-N AND HIS-RN INSERTS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT)1

DESIGN INFORMATION	Symbol	Units	Nomina	l Bolt/Ca <sub>l</sub> (in.) Fra	o Screw Dactional	iameter	Units	No	minal Bol (ı	t/Cap Scr nm) Metr		eter
			3/8	1/2	<sup>5</sup> / <sub>8</sub>	3/4		8	10	12	16	20
Effectiveness factor for	k	in-lb		1	7		SI			7.1		
cracked concrete	K <sub>c,cr</sub>	(SI)		(7	.1)		(in-lb)			(17)		
Effectiveness factor for	K <sub>c,uncr</sub>	in-lb		2	4		SI			10		
uncracked concrete	<b>N</b> c,uncr	(SI)		(1	0)	-	(in-lb)		÷.	(24)	÷.	-
Effective embedment depth	h <sub>ef</sub>	in.	43/8	5	63/4	8 <sup>1</sup> / <sub>8</sub>	mm	90	110	125	170	205
	Het	(mm)	(110)	(125)	(170)	(205)	(in.)	(3.5)	(4.3)	(4.9)	(6.7)	(8.1)
Min. anchor spacing <sup>3</sup>		in.	31/4	4	5	5 <sup>1</sup> / <sub>2</sub>	mm	63	83	102	127	140
win. anchor spacing	Smin	(mm)	(83)	(102)	(127)	(140)	(in.)	(2.5)	(3.25)	(4.0)	(5.0)	(5.5)
Min. edge distance <sup>3</sup>		in.	31/4	4	5	5 <sup>1</sup> / <sub>2</sub>	mm	63	83	102	127	140
wiiri. eage distance	C <sub>min</sub>	(mm)	(83)	(102)	(127)	(140)	(in.)	(2.5)	(3.25)	(4.0)	(5.0)	(5.5)
Minimum concrete	6	in.	5.9	6.7	9.1	10.6	mm	120	150	170	230	270
thickness	h <sub>min</sub>	(mm)	(150)	(170)	(230)	(270)	(in.)	(4.7)	(5.9)	(6.7)	(9.1)	(10.6)
Critical edge distance – splitting (for uncracked concrete)	Cac	-	See S	Section 4.1	.10 of this	report	-	S	See Sectio	n 4.1.10 o	f this repo	rt
Strength reduction factor for ension, concrete failure $\phi$ nodes <sup>2</sup>		-		0.	65		-			0.65		
Strength reduction factor for shear, concrete failure modes <sup>2</sup>	φ	-		0.	70		-			0.70		

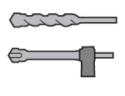
For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

<sup>&</sup>lt;sup>1</sup>Additional setting information is described in Figure 8A, Manufacturers Printed Installation Instructions (MPII). <sup>2</sup>The strength reduction factor applies when the load combinations from the IBC or ACI 318 are used and the requirements of ACI 318-19 17.5.3, ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are met. If the load combinations of ACI 318-11 Appendix C are used, the appropriate strength reduction factor must be determined in accordance with ACI 318-11 D.4.4.

<sup>&</sup>lt;sup>3</sup>For installations with 1<sup>3</sup>/<sub>4</sub>-inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.







Fractional and Metric HIS-N and HIS-RN **Internal Threaded Insert** 

Carbide Bit or Hilti Hollow Carbide Bit

#### TABLE 28—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL AND METRIC HILTI HIS-N AND HIS-RN INSERTS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT (OR HILTI HOLLOW CARBIDE DRILL BIT)1

DEGLON	INFOR		0	11.26	Nominal	bolt/cap s	crew dian	neter (in.)		Nor	ninal bolt/o	cap screw	diameter (r	mm)
DESIGN	INFOR	RMATION	Symbol	Units	3/8	1/2	5/8	3/4	Units	8	10	12	16	20
Embedm	ont		h <sub>ef</sub>	in.	4 <sup>3</sup> / <sub>8</sub>	5	6 <sup>3</sup> / <sub>4</sub>	8 <sup>1</sup> / <sub>8</sub>	mm	90	110	125	170	205
Embedii	ieni		Hef	(mm)	(110)	(125)	(170)	(205)	(in.)	(3.5)	(4.3)	(4.9)	(6.7)	(8.1)
	ē	Characteristic bond strength in cracked	_	psi	1,070	1,070	1,070	1,070	MPa	7.4	7.4	7.4	7.4	7.4
	ratu e A²	concrete	Tk,cr	(MPa)	(7.4)	(7.4)	(7.4)	(7.4)	(psi)	(1,070)	(1,070)	(1,070)	(1,070)	(1,070)
rete	Femperature range A <sup>2</sup>	Characteristic bond		psi	1,790	1,790	1,790	1,790	MPa	12.3	12.3	12.3	12.3	12.3
and	Te	strength in uncracked concrete	$\tau_{k,uncr}$	(MPa)	(12.3)	(12.3)	(12.3)	(12.3)	(psi)	(1,790)	(1,790)	(1,790)	(1,790)	(1,790)
rete	υ U	Characteristic bond		psi	740	740	740	740	MPa	5.1	5.1	5.1	5.1	5.1
Dry concrete and Water saturated concrete	Temperature range B <sup>2</sup>	strength in cracked concrete	Tk,cr	(MPa)	(5.1)	(5.1)	(5.1)	(5.1)	(psi)	(740)	(740)	(740)	(740)	(740)
Dry er s	mpe	Characteristic bond		psi	1,240	1,240	1,240	1,240	MPa	8.5	8.5	8.5	8.5	8.5
Wat	Je _	strength in uncracked concrete	$\tau_{k,uncr}$	(MPa)	(8.5)	(8.5)	(8.5)	(8.5)	(psi)	(1,240)	(1,240)	(1,240)	(1,240)	(1,240)
	Anchor	Category	-	-	1	1	1	1	-	1	1	1	1	1
	Streng	th Reduction factor	$\phi_{d,}\phi_{ws}$	-	0.65	0.65	0.65	0.65	1	0.65	0.65	0.65	0.65	0.65
	ē	Characteristic bond		psi	800	810	820	820	MPa	5.5	5.5	5.6	5.7	5.7
	Temperature range A²	strength in cracked concrete	Tk,cr	(MPa)	(5.5)	(5.6)	(5.7)	(5.7)	(psi)	(790)	(800)	(810)	(820)	(820)
	mpe	Characteristic bond		psi	1,340	1,350	1,370	1,380	MPa	9.1	9.2	9.3	9.5	9.5
hole	_ Te	strength in uncracked concrete	$\tau_{k,uncr}$	(MPa)	(9.2)	(9.3)	(9.5)	(9.5)	(psi)	(1,330)	(1,340)	(1,350)	(1,370)	(1,380)
led	ė	Characteristic bond		psi	550	560	570	570	MPa	3.8	3.8	3.8	3.9	3.9
Water-filled hole	Temperature range B²	strength in cracked concrete	Tk,cr	(MPa)	(3.8)	(3.8)	(3.9)	(3.9)	(psi)	(550)	(550)	(560)	(570)	(570)
× ×	empera range l	Characteristic bond		psi	920	930	950	950	MPa	6.3	6.4	6.4	6.5	6.6
	<u>e</u> –	strength in uncracked concrete	Tk,uncr	(MPa)	(6.4)	(6.4)	(6.5)	(6.6)	(psi)	(920)	(920)	(930)	(950)	(950)
	Anchor	Category	-	-	3	3	3	3	-	3	3	3	3	3
	Streng	th Reduction factor	$\phi_{ m wf}$	-	0.45	0.45	0.45	0.45	-	0.45	0.45	0.45	0.45	0.45
	ē	Characteristic bond strength in cracked	_	psi	710	720	750	750	MPa	4.8	4.9	5.0	5.1	5.2
	Temperature range A²	concrete	Tk,cr	(MPa)	(4.9)	(5.0)	(5.1)	(5.2)	(psi)	(700)	(710)	(720)	(750)	(750)
ę	mpe	Characteristic bond		psi	1,190	1,210	1,250	1,260	MPa	8.0	8.2	8.4	8.6	8.7
ncre	Te	strength in uncracked concrete	T <sub>k,uncr</sub>	(MPa)	(8.2)	(8.4)	(8.6)	(8.7)	(psi)	(1,160)	(1,190)	(1,210)	(1,250)	(1,260)
9 9	ė	Characteristic bond		psi	490	500	510	520	MPa	3.3	3.4	3.4	3.5	3.6
Submerged concrete	Temperature range B²	strength in cracked concrete	Tk,cr	(MPa)	(3.4)	(3.4)	(3.5)	(3.6)	(psi)	(480)	(490)	(500)	(510)	(520)
ubn	empera range l	Characteristic bond		psi	820	840	860	870	MPa	5.5	5.6	5.8	5.9	6.0
Ø	<u>e</u> –	strength in uncracked concrete	Tk,uncr	(MPa)	(5.6)	(5.8)	(5.9)	(6.0)	(psi)	(800)	(820)	(840)	(860)	(870)
	Anchor Category		-	-	3	3	3	3	-	3	3	3	3	3
	Streng	th Reduction factor	$\phi_{\sf uw}$	-	0.45	0.45	0.45	0.45	-	0.45	0.45	0.45	0.45	0.45
Reduction	on for se	eismic tension	αN,seis	-	1	1	1	1	-	1	1	1	1	1

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

<sup>1</sup>Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c / 2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c / 17.2)^{0.25}$ ] and  $(f_c / 2,500)^{0.15}$  for cracked concrete [For SI:  $(f_c / 17.2)^{0.15}$ ]. See Section 4.1.4 of this report for bond strength determination.

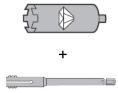
<sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







Fractional and Metric HIS-N and HIS-RN **Internal Threaded Insert** 

**Bond Strength** 

Diamond Core Bit + **Roughening Tool** 

#### TABLE 29—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL AND METRIC HILTI HIS-N AND HIS-RN INSERTS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL1

DESIG	N INFORMATIO	ON	Symbol	Units		al bolt/cap liameter (in		Units	Nominal bo	olt/cap scre (mm)	w diameter
					<sup>1</sup> / <sub>2</sub>	5/8	3/4		12	16	20
Embe	dmont		hef	in.	5	6¾	8 <sup>1</sup> / <sub>8</sub>	mm	125	170	205
LIIDE	ament		Tlet	(mm)	(125)	(170)	(205)	(in.)	(4.9)	(6.7)	(8.1)
-		Characteristic bond		psi	750	750	750	MPa	5.2	5.2	5.2
Saturated	Temperature	strength in cracked concrete	Tk,cr	(MPa)	(5.2)	(5.2)	(5.2)	(psi)	(750)	(750)	(750)
Satı	range A <sup>2</sup>	Characteristic bond		psi	1,790	1,790	1,790	MPa	12.3	12.3	12.3
ē		strength in uncracked concrete	Tk, uncr	(MPa)	(12.3)	(12.3)	(12.3)	(psi)	(1,790)	(1,790)	(1,790)
ie 🤉		Characteristic bond		psi	515	515	515	MPa	3.6	3.6	3.6
e and Water Concrete	Temperature	strength in cracked concrete	Tk,cr	(MPa)	(3.6)	(3.6)	(3.6)	(psi)	(515)	(515)	(515)
rete	range B <sup>2</sup>	Characteristic bond		psi	1,240	1,240	1,240	MPa	8.5	8.5	8.5
	range B <sup>2</sup> Characteristic bond strength in uncracked concrete		$ au_{k,uncr}$	(MPa)	(8.5)	(8.5)	(8.5)	(psi)	(1,240)	(1,240)	(1,240)
Dry	Anchor Categor	-	-	1	1	1	-	1	1	1	
	Strength Reduction factor			-	0.65	0.65	0.65	-	0.65	0.65	0.65
Reduc	tion for seismic t	ension	αN,seis	-	1	1	1	-	1	1	1

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.







Fractional and Metric HIS-N and HIS-RN Internal Threaded Insert

**Bond Strength** 

**Diamond Core Bit** 

#### TABLE 30—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL AND METRIC HILTI HIS-N AND HIS-RN INSERTS IN HOLES CORE DRILLED WITH A DIAMOND CORE BIT

			· ·	COKE DI	VILLED	WIIIIA	DIAMO	AD COK	L DII					
DESIG	N INFORMATIO	N	Symbol	Units	Nomina	l bolt/car (iı	screw d	liameter	Units	Nom	inal bolt/c	ap screw	diameter (	mm)
	3/8 1/2				5/8	3/4		8	10	12	16	20		
Embed	ment		h <sub>ef</sub>	in. (mm)	4 <sup>3</sup> / <sub>8</sub> (110)	5 (125)	6 <sup>3</sup> / <sub>4</sub> (170)	8 <sup>1</sup> / <sub>8</sub> (205)	mm (in.)	90 (3.5)	110 (4.3)	125 (4.9)	170 (6.7)	205 (8.1)
and Water Concrete	Temperature range A²	Characteristic bond strength in uncracked concrete	Tk,uncr	psi (MPa)	1,200 (8.3)	1,200 (8.3)	1,200 (8.3)	1,200 (8.3)	MPa (psi)	8.3 (1,200)	8.3 (1,200)	8.3 (1,200)	8.3 (1,200)	8.3 (1,200)
concrete an aturated Cor	Temperature range B <sup>2</sup>	Characteristic bond strength in uncracked concrete	Tk,uncr	psi (MPa)	830 (5.7)	830 (5.7)	830 (5.7)	830 (5.7)	MPa (psi)	5.7 (830)	5.7 (830)	5.7 (830)	5.7 (830)	5.7 (830)
ည်လိ	≥ ശ് Anchor Category		-	-	3	3	3	3	-	2	3	3	3	3
	Strength Reduc	tion factor	φ <sub>d</sub> , φ <sub>ws</sub>	-	0.45	0.45	0.45	0.45	-	0.55	0.45	0.45	0.45	0.45

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Bond strength values correspond to concrete compressive strength  $f_c$  = 2,500 psi (17.2 MPa). For concrete compressive strength,  $f_c$ , between 2,500 psi (17.2 MPa) and 8,000 psi (55.2 MPa), the tabulated characteristic bond strength may be increased by a factor of  $(f_c / 2,500)^{0.25}$  for uncracked concrete [For SI:  $(f_c / 17.2)^{0.25}$ ]. See Section 4.1.4 of this report for bond strength determination.

 $<sup>^{1}</sup>$ Bond strength values correspond to concrete compressive strength in the range 2,500 psi ≤ f'c ≤ 8,000 psi.  $^{2}$ Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C). Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

<sup>&</sup>lt;sup>2</sup>Temperature range A: Maximum short term temperature = 130°F (55°C), Maximum long term temperature = 110°F (43°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), Maximum long term temperature = 110°F (43°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

TABLE 31—DEVELOPMENT LENGTH FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR HILTI HOLLOW CARBIDE BIT OR CORE DRILLED WITH A DIAMOND CORE BIT OR A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL 1.2.5,6

							Bar	Size			
DESIGN INFORMATION	Symbol	Criteria Section of Reference Standard	Units	#3	#4	#5	#6	#7	#8	#9	#10
Nominal reinforcing	dь	ASTM A615/A706	in.	0.375	0.500	0.625	0.750	0.875	1.000	1.128	1.270
bar diameter	αь	A51W A015/A700	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(28.7)	(32.3)
Nominal bar area	4	ACTM AC45/A706	in <sup>2</sup>	0.11	0.20	0.31	0.44	0.60	0.79	1.00	1.27
Nominal par area	Ab	ASTM A615/A706	(mm²)	(71)	(129)	(199)	(284)	(387)	(510)	(645)	(819)
Development length for $f_y = 60$ ksi and $f_c = 2,500$ psi (normal)		ACI 318-19 25.4.2.4 ACI 318-14 25.4.2.3 ACI 318-11 12.2.3	in.	12.0	14.4	18.0	21.6	31.5	36.0	40.6	45.7
weight concrete)3,4		7.01.010-11 12.2.0	(mm)	(304.8)	(365.8)	(457.2)	(548.6)	(800.1)	(914.4)	(1031.4)	(1161.3)
Development length for $f_y$ = 60 ksi and $f'_c$ = 4,000 psi (normal		ACI 318-19 25.4.2.4 ACI 318-14 25.4.2.3	in.	12.0	12.0	14.2	17.1	24.9	28.5	32.1	36.1
weight concrete) <sup>3,4</sup>		ACI 318-11 12.2.3	(mm)	(304.8)	(304.8)	(361.4)	(433.7)	(632.5)	(722.9)	(815.4)	(918.1)

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

TABLE 32—DEVELOPMENT LENGTH FOR EU METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR HILTI HOLLOW CARBIDE BIT OR CORE DRILLED WITH A DIAMOND CORE BIT OR A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL 1,2,5,6

		ROUGHENED WI	III A IIIL	. II KOUGH		, <u> </u>			
		Criteria Section of				Bar	Size		
DESIGN INFORMATION	Symbol	Reference Standard	Units	10	12	16	20	25	32
Nominal reinforcing bar	$d_b$	BS4449: 2005	mm	10	12	16	20	25	32
diameter	αь	B34449. 2003	(in.)	(0.394)	(0.472)	(0.630)	(0.787)	(0.984)	(1.260)
Naminal har area	Ab	BS 4449: 2005	mm <sup>2</sup>	78.5	113.1	201.1	314.2	490.9	804.2
Nominal bar area	Аь	BS 4449: 2005	(in²)	(0.12)	(0.18)	(0.31)	(0.49)	(0.76)	(1.25)
Development length for $f_y = 72.5$ ksi and $f'_c = 2,500$	I <sub>d</sub>	ACI 318-19 25.4.2.4 <sup>7</sup> ACI 318-14 25.4.2.3	mm	348	417	556	871	1087	1392
psi (normal weight concrete) <sup>3,4</sup>	ņ	ACI 318-11 12.2.3	(in.)	(13.7)	(16.4)	(21.9)	(34.3)	(42.8)	(54.8)
Development length for $f_v = 72.5$ ksi and $f'_c = 4,000$	I <sub>d</sub>	ACI 318-19 25.4.2.4 <sup>7</sup> ACI 318-14 25.4.2.3	mm	305	330	439	688	859	1100
psi (normal weight concrete) <sup>3,4</sup>	Id	ACI 318-11 12.2.3	(in.)	(12.0)	(13.0)	(17.3)	(27.1)	(33.8)	(43.3)

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

<sup>&</sup>lt;sup>1</sup>Development lengths valid for static, wind, and earthquake loads (SDC A and B).

<sup>&</sup>lt;sup>2</sup>Development lengths in SDC C through F must comply with ACI 318 (-19 or -14) Chapter 18 or ACI 318-11 Chapter 21, as applicable, and section 4.2.4 of this report.

<sup>&</sup>lt;sup>3</sup> For all-lightweight concrete, increase development length by 33% unless the provisions of ACI 318-19 25.4.2.5 or ACI 318-14 25.4.2.4 are met to permit λ > 0.75. For sand-lightweight concrete, increase development length by 18% unless the provisions of ACI 318-19 25.4.2.5 or ACI 318-14 25.4.2.4 are met to permit λ > 0.85.

 $<sup>4\</sup>left(\frac{c_b + K_{tr}}{d_{s}}\right) = 2.5, \ \psi_t = 1.0, \ \psi_e = 1.0, \ \psi_s = 0.8 \ \text{for } d_b \le \#6, 1.0 \ \text{for } d_b > \#6$ 

<sup>&</sup>lt;sup>5</sup>Calculations may be performed for other steel grades per ACI 318 (-19 or -14) Chapter 25 or ACI 318-11 Chapter 12.

<sup>&</sup>lt;sup>6</sup>Minimum development length shall not be less than 12 in (305 mm) per ACI 318 (-19 or -14) Section 25.4.2.1.

<sup>&</sup>lt;sup>1</sup>Development lengths valid for static, wind, and earthquake loads (SDC A and B).

<sup>&</sup>lt;sup>2</sup>Development lengths in SDC C through F must comply with ACI 318 (-19 or -14) Chapter 18 or ACI 318-11 Chapter 21 and section 4.2.4 of this report.

<sup>&</sup>lt;sup>3</sup> For all-lightweight concrete, increase development length by 33% unless the provisions of ACI 318-19 25.4.2.5 or ACI 318-14 25.4.2.4 are met to permit λ > 0.75. For sand-lightweight concrete, increase development length by 18% unless the provisions of ACI 318-19 25.4.2.5 or ACI 318-14 25.4.2.4 are met to permit λ > 0.85.

 $<sup>4\</sup>left(\frac{c_b + K_{tr}}{dt}\right) = 2.5, \ \psi_t = 1.0, \ \psi_e = 1.0, \ \psi_s = 0.8 \ \text{for } d_b < 20 \ \text{mm}, 1.0 \ \text{for } d_b \ge 20 \ \text{mm}$ 

<sup>&</sup>lt;sup>5</sup>Calculations may be performed for other steel grades per ACI 318 (-19 or -14) Chapter 25 or ACI 318-11 Chapter 12.

<sup>&</sup>lt;sup>6</sup>Minimum development length shall not be less than 12 in (305 mm) per ACI 318 (-19 or -14) Section 25.4.2.1.

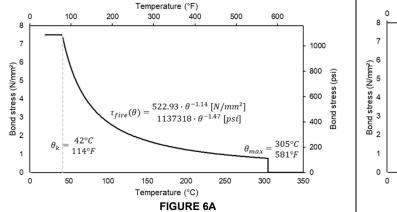
<sup>&</sup>lt;sup>7</sup> I<sub>d</sub> must be increased by 9.5% to account for  $\psi_g$  in ACI 318-19 25.4.2.4.  $\psi_g$  has been interpolated from Table 25.4.2.5 of ACI 318-19 for f<sub>y</sub> = 72.5 ksi.

TABLE 33—DEVELOPMENT LENGTH FOR CANADIAN REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT OR HILTI HOLLOW CARBIDE BIT OR CORE DRILLED WITH A DIAMOND CORE BIT OR A DIAMOND CORE BIT AND ROUGHENED WITH A HILTI ROUGHENING TOOL 1,2,5,6

		WIIII A IIIE II						
		Criteria Section of Reference				Bar Size		
DESIGN INFORMATION	Symbol	Standard	Units	10M	15M	20M	25M	30M
Nominal reinforcing bar	<b>d</b> b	CAN/CSA-G30.18 Gr.400	mm	11.3	16.0	19.5	25.2	29.9
diameter	u <sub>b</sub>	CAN/00A-000.10 G1.400	(in.)	(0.445)	(0.630)	(0.768)	(0.992)	(1.177)
Naminal kanana	4	CAN/OCA C30 40 C- 400	mm <sup>2</sup>	100.3	201.1	298.6	498.8	702.2
Nominal bar area	$A_b$	CAN/CSA-G30.18 Gr.400	(in²)	(0.16)	(0.31)	(0.46)	(0.77)	(1.09)
Development length for $f_y = 58$ ksi and $f'_c = 2,500$ psi	I <sub>d</sub>	ACI 318-19 25.4.2.4 ACI 318-14 25.4.2.3	mm	315	445	678	876	1,041
(normal weight concrete) <sup>3,4</sup>		ACI 318-11 12.2.3	(in.)	(12.4)	(17.5)	(26.7)	(34.5)	(41.0)
Development length for $f_y = 58$ ksi and $f_c = 4,000$ psi (normal weight concrete) <sup>3,4</sup>	I <sub>d</sub>	ACI 318-19 25.4.2.4 ACI 318-14 25.4.2.3	mm	305	353	536	693	823
(normal weight concrete)		ACI 318-11 12.2.3	(in.)	(12.0)	(13.9)	(21.1)	(27.3)	(32.4)

For **SI**: 1 inch  $\equiv$  25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

<sup>&</sup>lt;sup>6</sup>Minimum development length shall not be less than 12 in (305 mm) per ACI 318 (-19 or -14) Section 25.4.2.1.



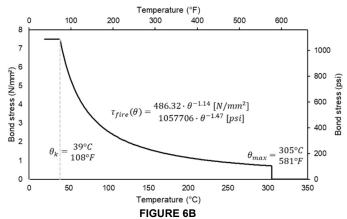


FIGURE 6 – BOND STRESS VS TEMPERATURE OF POST INSTALLED REINFORCING BAR APPLICATIONS SUBJECT TO ELEVATED TEMPERATURE / FIRE.
FIGURE 6A FOR SHORT TERM LOADS INCLUDING SEISMIC; FIGURE 6B FOR SUSTAINED LOADS INCLUDING SEISMIC

<sup>&</sup>lt;sup>1</sup>Development lengths valid for static, wind, and earthquake loads (SDC A and B).

<sup>&</sup>lt;sup>2</sup>Development lengths in SDC C through F must comply with ACI 318 (-19 or -14) Chapter 18 or ACI 318-11 Chapter 21 and section 4.2.4 of this report.

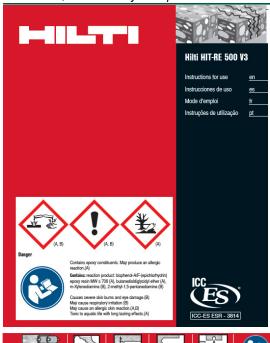
<sup>&</sup>lt;sup>3</sup> For all-lightweight concrete, increase development length by 33% unless the provisions of ACI 318-19 25.4.2.5 or ACI 318-14 25.4.2.4 are met to permit λ > 0.75. For sand-lightweight concrete, increase development length by 18% unless the provisions of ACI 318-19 25.4.2.5 or ACI 318-14 25.4.2.4 are met to permit λ > 0.85.

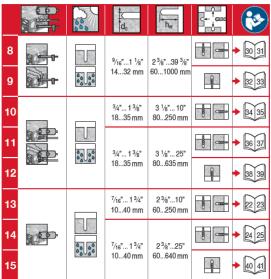
 $<sup>4\</sup>left(\frac{c_b + K_{tr}}{dt}\right) = 2.5, \ \psi_l = 1.0, \ \psi_e = 1.0, \ \psi_s = 0.8 \ \text{for } d_b < 20\text{M}, 1.0 \ \text{for } d_b \ge 20\text{M}$ 

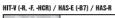
<sup>&</sup>lt;sup>5</sup>Calculations may be performed for other steel grades per ACI 318 (-19 or -14) Chapter 25 or ACI 318-11 Chapter 12.

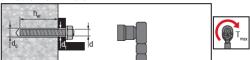


FIGURE 7—HILTI HIT-RE 500 V3 ANCHORING SYSTEM









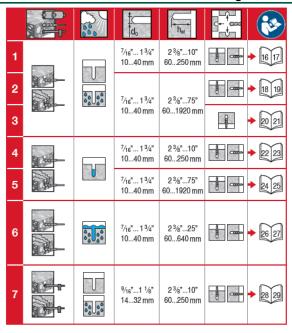
HAS / HIT-V

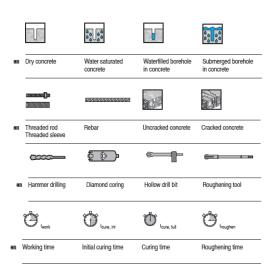
	Ø d₀	h <sub>ef</sub>	Ø d <sub>f</sub>	T <sub>max</sub>	T <sub>max</sub>
Ø d [inch]	[inch]	[inch]	[inch]	[ft-lb]	[Nm]
3/8	7/16	23/871/2	7/16	15	20
1/2	9/16	23/410	9/16	30	41
5/8	3/4	3 1/8 12 1/2	11/16	60	81
3/4	7/8	31/215	13/16	100	136
7/8	1	3 1/2 17 1/2	15/16	125	169
1	1 1/8	420	1 ½	150	203
1 1/4	13/8	525	13/8	200	271

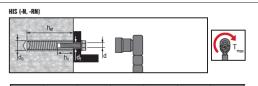
#### HIT-V

executed to	Ø d₀		Ø d <sub>f</sub>	T <sub>max</sub>
Ø d [mm]	[mm]	[mm]	[mm]	[Nm]
M8	10	60160	9	10
M10	12	60200	12	20
M12	14	70240	14	40
M16	18	80320	18	80
M20	22	90400	22	150
M24	28	100480	26	200
M27	30	110540	30	270
M30	35	120600	33	300

1 inch = 25,4 mm



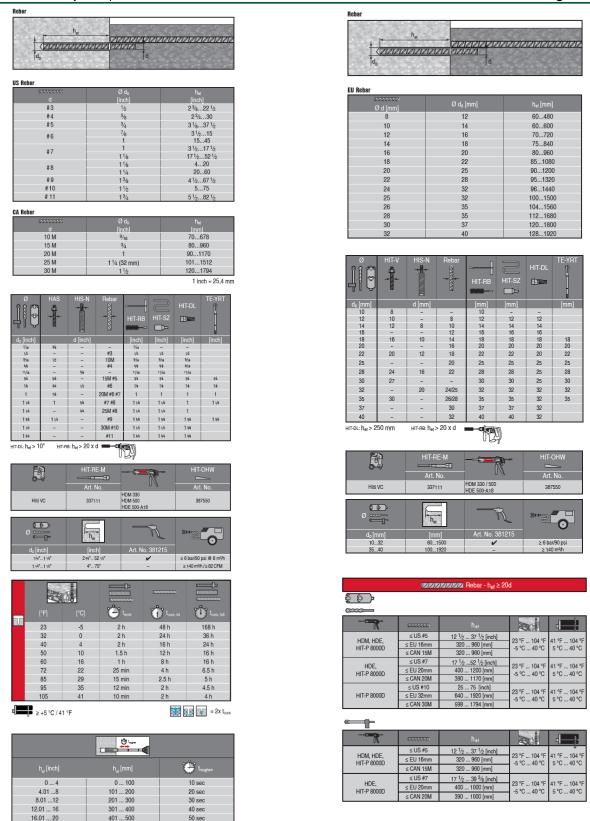


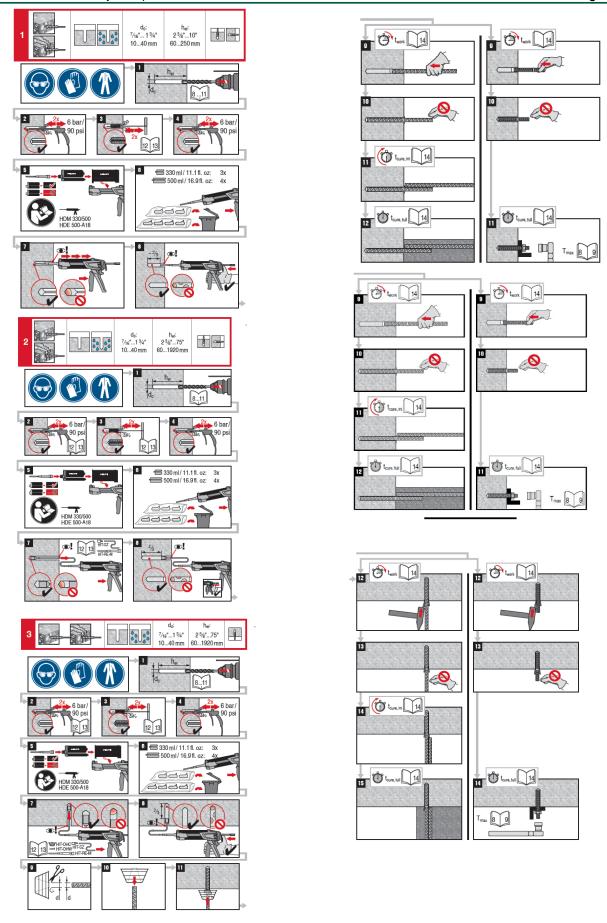


Ø d [inch]	Ø d₀ [inch]	h <sub>ef</sub> [inch]	Ø d <sub>f</sub> [inch]	h₅ [inch]	T <sub>max</sub> [ft-lb]	T <sub>max</sub> [Nm]
3/8	11/16	43/8	7/16	3/815/16	15	20
1/2	7/8	5	9/16	1/21 3/16	30	41
5/8	1 1/8	63/4	11/16	5/81 1/2	60	81
3/4	1 1/4	81/8	13/16	3/417/8	100	136

Ø d [mm]	Ø d₀ [mm]	h <sub>er</sub> [mm]	Ø d <sub>f</sub> [mm]	hs [mm]	T <sub>max</sub> [Nm]
M8	14	90	9	820	10
M10	18	110	12	1025	20
M12	22	125	14	1230	40
M16	28	170	18	1640	80
M20	32	205	22	2050	150

nen = hef [inch] \* 2.5





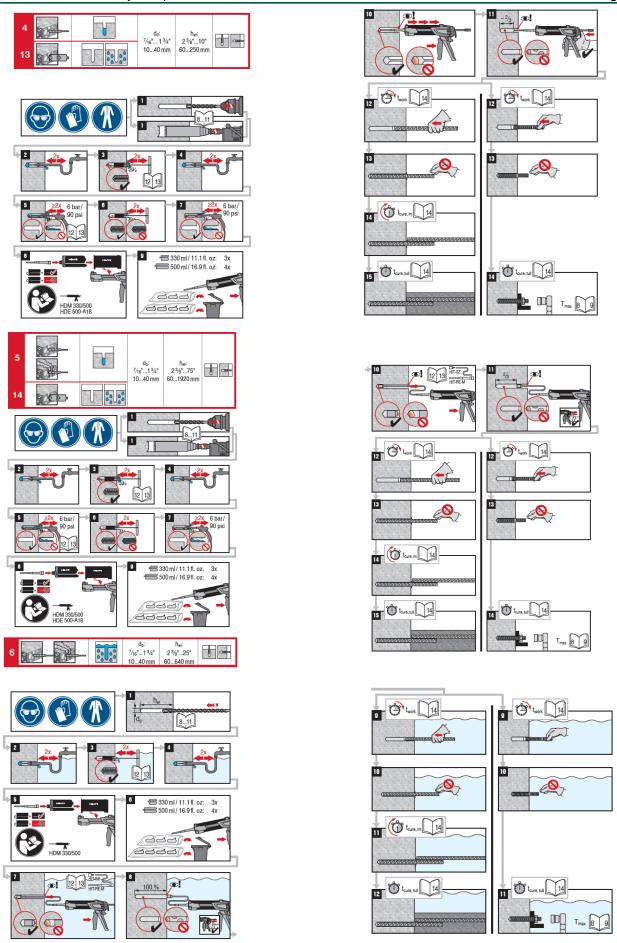


FIGURE 8A—MANUFACTURER'S PRINTED INSTALLATION INSTRUCTIONS (MPII) (Continued)

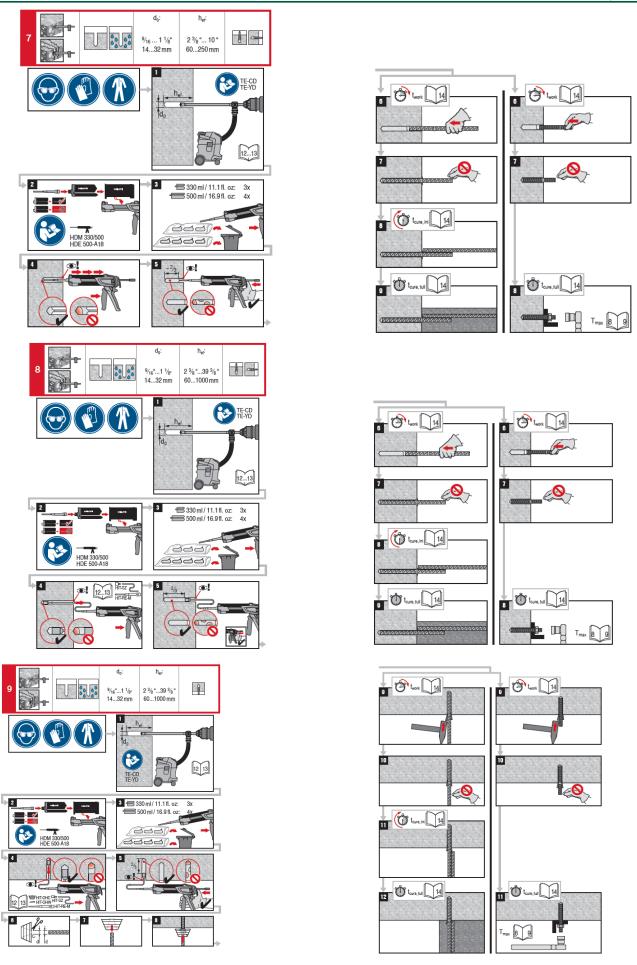


FIGURE 8A—MANUFACTURER'S PRINTED INSTALLATION INSTRUCTIONS (MPII) (Continued)

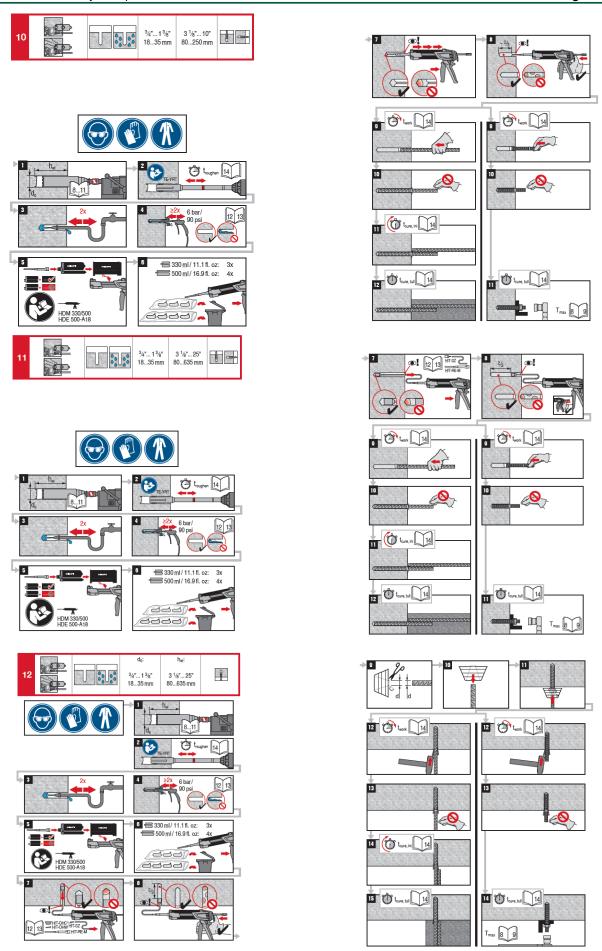
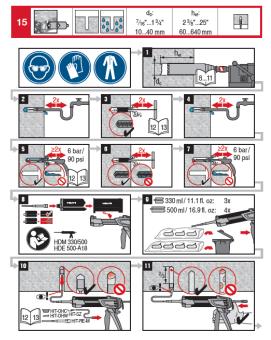


FIGURE 8A—MANUFACTURER'S PRINTED INSTALLATION INSTRUCTIONS (MPII) (Continued)

en



Adhesive anchoring system for rebar and anchor fastenings in concrete

► Prior to use of product, follow the instructions for use and the legally obligated safety precautions.

► See the Safety Data Sheet for this product.

#### HIH HIT-RE 500 V3

Contains epoxy constituents. May produce an altergic reaction.(A)

Gentains: reaction product bisphenck-AF-(e)pichlorhydrin) epoxy resin MW ≤ 700 (A), butanedioldiglycidyl ether (A),

m-Xylenedamine (B), 2-metlyl+1, 5-pentanediamine (A).



Wear protective gloves/protective clothing/eye protection/face protection Do not breathe vapours.

IF ON SKIN (or hair): Remove/Take off immediately all contaminated clothing. Rinse skin with

water/armower.
P305+P501+P308 IP IN EYES: Rince caudiously with water for several minutes. Remove contact lenses, if present and easy to do. Continue rinsing.
P333+P313 If skin irritation re-and occurs: Cell medical advice/altention.
If eye irritation persists: Get medical advice/altention.

Recommended protective: equipment:
For protective: Equipment:
For protective: Trighty sealed salety glasses e.g.: e00055440 Salety glasses PP EY-CA NCH clear;
R00055551 Gogger PE-EY-HA R HCAFF clear;
Protective glasses: EN 374; Material of gloves: Nitrie nober, NSR
Avoid direct contact with the Americal the product the preparation by organizational measures.
Final selection as superprotective protective: equipment is in the respectability of the sizer

#### Disposal considerations

➤ Leave the Mixer attached and dispose of via the local Green Dot collecting system

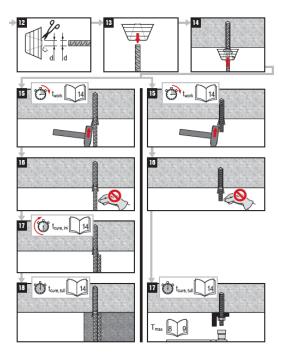
— or EAK waste material code 15 01 02 plastic packaging.

Fall or partially empticed packs:

dispose of as special waste in accordance with official regulations.

EAK waste material code: 20 of 27° paint, inits, adhesives and resins containing dangerous substances.

or waste material code: EAK 060 + 06° waste adhesives and sealants containing organic solvents or other dangerous



Warranty: Refer to standard Hillt terms and conditions of sale for warranty information

Failure to observe these installation instructions, use of non-Hilli anchors, poor or questionable concrete conditions, or unique applications may affect the reliability or performance of the fastenings.

- Always keep bit instruction for use together with the product.

  Ensure that the instruction for use is with the product when it is given to other persons.

  Satchy Bash Saterf, Have When DB below use.

  Clack capitalise date: See expiration date imprint on folgoack manifold (month/year). Do not use expired product feel pack femperature during waspet +5° Ct to 40° Cf 14° Fe' to 194 °F.

  Genefities for transport and storage: Keep in a cool, dry and dark place between +5° Ct to 25° Cf.
- \*1 T to // T\*.

  For any application not covered by this document / beyond values specified, please contact Hills.

  Farly sucd fell packs must be used up within 4 weeks. Leave the mixer attached on the foll pack manifold and store under the recommended storage conditions. If reused, attach a new mixer and discard the initial quantity of anchor adherive.

- L3 vendama

  ▲ Improper handling may cases mertar splashes. Eye contact with mertar may cases irreversible sye damaged

   Always were tightly leaded salely glasses, gloves and prolective clothes before handling the mortar!

   Never last dispensing without a mixer properly screwed on.

   When cuttand sectional hose liveract of initial mortar flow must be done through supplied mixer only (not through the setentiation hose).

   Allash a new mixer port of dispensing a new foil pack (snos fill).
- The extension most prior to dispensing a new foil pack (snug fit).

   Caution! Never remove the mixer while the foil pack system is under pressure. Press the release button of the

- Caution Never remove the mixer while the foll pack system is under pressure. Press the release button of the dispenser to under motar splanting.

   Use only the type of mixer supplied with the adhesive. Do not modify the mixer in any way.

   Never use damaged foil packs and/or damaged or unclean foil pack holders.

  ▲ Pear load values / putential failure or flacturing paints due to inadequate benefic cleaning. The berefules must be dry and firer of debris, dust, water, it, or use and other containings in pair to adhesive including.

   For binding out the bondhele blood out with oil the ear until return air steam is fire of noticeable dust.

   For flushing the borehole flush with water line pressure until water runs clear.

   Important Remove all water from the bonehole and bow out with oil the ear time compressed air until bonehole is completely dried before mortar injection (not applicable to harmer drilled hole in underwater application).

   A fearer that betwelcts are filled from the back of the benefices without terming air veids.

- used without how a specific from the back of the berelaists without farming air widt.

  If necessary use the accessories of extensions to reach the back of the bondhole.

  For overhead applications use the overhead accessories if IFT 2, IFF and talk as special care when inserting the fast-ning atems. Excess adherior may be forced out of the bondhole. Back sure that no motion drips only the installar, IFF are in the production of the production of the special care when it is native to the installar of its a previously-special foil part, the first figger goal form the discarded.
- If a new mixer is installed onto a previously-opened
   A new mixer must be used for each new foil pack.

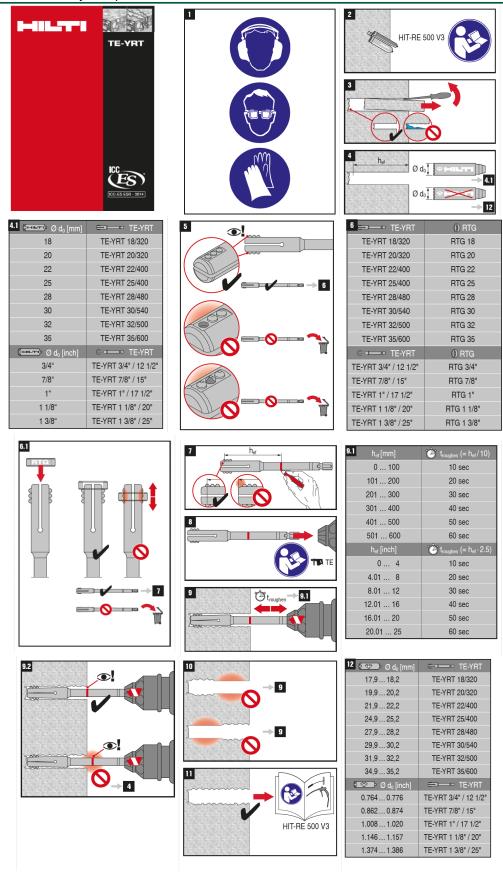


FIGURE 8B—MANUFACTURER'S PRINTED INSTALLATION INSTRUCTIONS (MPII)



### **ICC-ES Evaluation Report**

### **ESR-3814 LABC and LARC Supplement**

Reissued January 2023 Revised March 2023 This report is subject to renewal January 2025.

www.icc-es.org | (800) 423-6587 | (562) 699-0543

A Subsidiary of the International Code Council®

**DIVISION: 03 00 00—CONCRETE** Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

HILTI, INC.

#### **EVALUATION SUBJECT:**

HILTI HIT-RE 500 V3 ADHESIVE ANCHORS AND POST-INSTALLED REINFORCING BAR CONNECTIONS IN CRACKED AND UNCRACKED CONCRETE

#### 1.0 REPORT PURPOSE AND SCOPE

#### Purpose:

The purpose of this evaluation report supplement is to indicate that the Hilti HIT RE 500 V3 Adhesive Anchoring System and Post-Installed Reinforcing Bar System for cracked and uncracked concrete, described in ICC-ES evaluation report ESR-3814, has also been evaluated for compliance with the codes noted below as adopted by the Los Angeles Department of Building and Safety (LADBS).

#### Applicable code editions:

- 2020 City of Los Angeles Building Code (LABC)
- 2020 City of Los Angeles Residential Code (LARC)

#### 2.0 CONCLUSIONS

The Hilti HIT-RE 500 V3 Adhesive Anchoring System and Post-Installed Reinforcing Bar System for cracked and uncracked concrete, described in Sections 2.0 through 7.0 of the evaluation report ESR-3814, complies with LABC Chapter 19, and LARC, and is subject to the conditions of use described in this supplement.

#### 3.0 CONDITIONS OF USE

The Hilti HIT RE 500 V3 Adhesive Anchoring System and Post-Installed Reinforcing Bar System described in this evaluation report supplement must comply with all of the following conditions:

- All applicable sections in the evaluation report ESR-3814.
- The design, installation, conditions of use and labeling of the Hilti HIT-RE 500 V3 Adhesive Anchoring System and Post-Installed Reinforcing Bar System are in accordance with the 2018 International Building Code® (IBC) provisions noted in the evaluation report ESR-3814.
- The design, installation and inspection are in accordance with additional requirements of LABC Chapters 16 and 17, as
- Under the LARC, an engineered design in accordance with LARC Section R301.1.3 must be submitted.
- The allowable and strength design values listed in the evaluation report and tables are for the connection of the adhesive anchors and post installed reinforcing bars to the concrete. The connection between the adhesive anchors or post installed reinforcing bars and the connected members shall be checked for capacity (which may govern).
- For use in wall anchorage assemblies to flexible diaphragm, anchors shall be designed per the requirements of City of Los Angeles Information Bulletin P/BC 2020-071.

This supplement expires concurrently with the evaluation report, reissued January 2023 and revised March 2023.







### **ICC-ES Evaluation Report**

### **ESR-3814 FBC Supplement**

Reissued January 2023 Revised March 2023 This report is subject to renewal January 2025.

www.icc-es.org | (800) 423-6587 | (562) 699-0543

A Subsidiary of the International Code Council®

DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

**DIVISION: 05 00 00—METALS** 

Section: 05 05 19—Post-Installed Concrete Anchors

**REPORT HOLDER:** 

HILTI, INC.

#### **EVALUATION SUBJECT:**

HILTI HIT-RE 500 V3 ADHESIVE ANCHORS AND POST-INSTALLED REINFORCING BAR CONNECTIONS IN CRACKED AND UNCRACKED CONCRETE

#### 1.0 REPORT PURPOSE AND SCOPE

#### Purpose:

The purpose of this evaluation report supplement is to indicate that the Hilti HIT-RE 500 V3 Adhesive Anchors and Post-Installed Reinforcing Bar System in Concrete, described in ICC-ES evaluation report ESR-3814, has also been evaluated for compliance with the codes noted below.

#### Applicable code editions:

- 2020 Florida Building Code—Building
- 2020 Florida Building Code—Residential

#### 2.0 CONCLUSIONS

The Hilti HIT-RE 500 V3 Adhesive Anchor System and Post-Installed Reinforcing Bar System, described in Sections 2.0 through 7.0 of ICC-ES evaluation report ESR-3814, comply with the *Florida Building Code—Building* and the *Florida Building Code—Residential*, provided the design requirements are determined in accordance with the *Florida Building Code—Building Code—Residential*, as applicable. The installation requirements noted in ICC-ES evaluation report ESR-3814 for the 2018 *International Building Code®* meet the requirements of the *Florida Building Code—Building* or the *Florida Building Code—Residential*, as applicable.

Use of the Hilti HIT-RE 500 V3 Adhesive Anchor System and Post-Installed Reinforcing Bar System has also been found to be in compliance with the High-Velocity Hurricane Zone provisions of the *Florida Building Code—Building* and the *Florida Building Code—Residential* with the following condition.

 For anchorage of wood members, the connection subject to uplift, must be designed for no less than 700 pounds (3114 N).

For products falling under Florida Rule 61G20-3, verification that the report holder's quality-assurance program is audited by a quality-assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official, when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the evaluation report, reissued January 2023 and revised March 2023.

